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# Pressurized Liquid Extraction of Hemp Residue and Purification of the Extract with Liquid-Liquid Extraction

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#### Abstract

The first semi-continuous Pressurized Liquid Extraction (PLE) of hemp threshing residue with ethanol was carried out according to a 3<sup>2</sup> full factorial experimental design with pressure and temperature as independent variables at 8-10-12 MPa and 323-333-343 K, respectively. The total- and cannabidiol (CBD) yield curves were fitted to the modified two-parameter Brunner equation. Best results, concerning CBD, can be achieved at 12 MPa and 343 K. Solvent mass-consumption and operation time were considerably decreased compared to a previous supercritical fluid extraction study on the same material. Furthermore, the concentration profiles were evaluated to study the mass transfer. The winterized dry extracts were further studied in a methanol-hexane-water ternary system concerning CBD distribution ratio, showing high methanol dependency.

#### Keywords

hemp threshing residue, solid-liquid extraction, PLE, CBD, distribution coefficient, ternary mixture

#### **1** Introduction

*Cannabis sativa* L. is a well-known plant for either as textile fiber or its recreational use. The origin of it is most likely in Central North-East Asia [1]. As fiber material, it is proved to be at least 5000 years old. Knowledge on its psychotropic effect dates back 2200 years in one of the oldest pharmacopeias, the Pen-ts'ao Ching, states the excessive use of the "fruits of hemp" causes hallucinations, precisely: "seeing devils" [2].

Due to human impact, two main phenotypes had developed from the species. One is marijuana a highly psychoactive and the other is industrial hemp a fiber-type variety. Both phenotypes are bioresource of phytocannabinoids – a diverse group of isoprenylated polyketides. [3] There are more than 90 cannabinoids that can be present in the plant. Practical classification differentiates two groups: psychotropic cannabinoids (PC) and non-psychotropic cannabinoids (NPC).  $\Delta^9$ -tetrahydrocannabinol ( $\Delta^9$ -THC), its acid (THCA), and its oxidized form cannabinol (CBN) are the most charted PC compounds. Cannabidiol (CBD), its acid (CBDA), are the most influential NPCs. The composition of the cannabinoid profile of each plant phenotypes can vary to a great extent on weather and soil conditions [4–6]. Psychoactive-type cultivation focuses on PC enrichment in the plant. Industrial hemp – classification criteria:  $\Delta^{9}$ -THC content is lower than 0.3 w/w%; EU legislation [7] is mainly considered a fiber source [4, 6]. It represents a high-quality fiber that is adequate for several industries such as the automotive industry, bio-building, paper manufacturing, and textile industry [6, 8].

In the fiber processing industry the inflorescences, leaves, and thin stems are called the threshing residue which is usually discarded or used for animal bedding – however, there are examples where the seeds are also considered as a waste [9]. These remaining waste materials might represent an opportunity. A study estimated that during seed harvest and seed cleaning 2 t/ha residue can be collected [5]. In another study, at a fiber production facility, lost hemp dust was evaluated to be 18–33 w/w% of the raw material [10]. These different residues contain several valuable components like sugars, alkaloids, quinones [10], and NPCs – some of which are specific to the genus *Cannabis* [3].

The aforementioned cannabidiol (CBD) has become the subject of considerable interest in recent years. Several studies proved its therapeutic effect for the treatment of the central nervous system, peripheral disorder, pain, and epilepsy without any psychotropic effect [11–14].

As fiber type hemp varieties are convenient sources of CBD, several studies were conducted to obtain it from the various parts of the harvested plant. Besides, antioxidants, aromas, essential oils, fatty acids etc. were also found in significant quantities [13–24]. However, in the practical application, the separation of solid fractions (e.g., inflorescences from leaves) is highly time-consuming and also unfavorable for the low-cost agricultural industry. In response, some recent studies focus on combined threshing residue extraction [4, 25–28], or stage-wise extraction of waste materials with respect to different fiber production units [8]. These separation processes are all based on solid-liquid or fluid extractions and mainly with batch operation.

Commonly used solvents for hemp extractions were methanol, ethanol, hexane, acetone, and supercritical carbon dioxide ( $scCO_2$ ). In some cases, water or ethanol is added as a co-solvent. Solubility data is scarce since the composition and concentration profile of the same plant type varies yearly. Therefore the solubility data in these studies might contradict extraction data due to the matrix effect.

Several techniques are available for enhanced separation such as accelerated solvent extraction [29], microwaveor ultrasound-assisted extraction [15, 30], and Pressurized Liquid Extraction (PLE) for hemp extraction [31, 32]. From these techniques, the most promising for continuous or semi-continuous operation is the PLE.

Serna-Ioaiza et al. [32] carried out a three-step upscaling of hemp threshing residue extraction. A two-cycle batch PLE study was conducted at pressures (P) of 5–10–15 MPa, and temperatures (T) at 323–348 K with a liquid-to-solid mass ratio of 3.3–5. Two-cycle extraction was rejected due to the low amount recovered in the second step. A twoway ANOVA of the extracts showed that the pressure did not influence either the CBD or  $\Delta^9$ -THC yields. Optimal extraction time in the PLE section was estimated between 10–100 min.

In another example, Kitrytė et al. [31] biorefined hemp threshing residue with consecutive supercritical carbon dioxide extraction, acetone PLE, water-ethanol PLE, and enzyme-assisted extraction. The best operational conditions of each stage were determined, and a thorough analysis of the products was reported for each stage. The optimal parameters of both PLE experiments were found to be 10.3 MPa and 373 K for 45 min while liquid to solid ratio was not specified.

In this study, the first semi-continuous PLE was carried out on hemp threshing residue with absolute ethanol. Two different total extraction times were examined. The mass-transfer kinetics was further studied by evaluation of the concentration profiles. After evaluation of the PLE experimental design, the extracts were combined into a bulk, winterized, mixed then separated into five uniform parts. In five different hexane-methanol-water system the extracts were separately redissolved. The distribution ratio of CBD in theses systems was analyzed to further investigate the possible purification options of CBD from the crude extract.

# 2 Materials and methods

### 2.1 Materials

For the measurements, acetonitrile (CAS: 75-05-8, purity: > 99.0 %), absolute ethanol (CAS: 64-15-5, purity:  $\geq$  99.5 %), methanol (CAS: 67-56-1; purity:  $\geq$  99.5 %), and hexane (CAS: 110-54-3, purity:  $\geq$  95.0 %) were purchased from Merck Millipore Ltd. (Budapest, Hungary). The ammonium-acetate (CAS: 631-61-8, purity:  $\geq$  97 %) and acetic-acid (CAS: 64-19-7, purity:  $\geq$  96.0 %) were purchased from Molar Chemicals Ltd. (Budapest, Hungary). Water was locally distilled with an electric conductivity of 0.1 mS/cm. For filtration 0.02 µm Whatman<sup>TM</sup> Anotop<sup>TM</sup> inorganic (alumina based) membrane filter (syringe filter) was purchased from Merck. For winterization a glass filter was used with 10–16 µm porosity.

The industrial hemp phenotype was previously the subject of another study of our research group (marked as Sample 5) [25]. It is a fiber-type variaty harvested in 2013 with a moisture content of  $11.0 \pm 0.1$  (w/w%). The particle size is  $0.50 \pm 0.01$  mm with a uniformity factor of  $2.05 \pm 0.06$ . Total CBD content was evaluated to be  $782 \pm 32$  mg /100 g of dry material by Soxhlet extraction with acetonitrile.

# 2.2 Methods

### 2.2.1 PLE experiments

The Pressurized Liquid Extraction setup can be seen in Fig. 1. A  $\frac{1}{2}$  stainless steel tube is used as an extractor. LKB Bromma 2150 HPLC pump is employed to provide the constant volumetric ethanol flow of 1.5 mL/min a 3 m long 1/16' stainless steel capillary is connecting the extractor and the liquid pump.

After filling the extractor with approximately 7 g of threshing residue, the tube was closed with cotton balls on both ends then connected to the 1/16' capillary and preheated for 5 min in the water bath. The maximal flow rate (5.00 mL/min) was used to fill the extractor rapidly. After the first few drops, the regulating valve was closed until pressure build-up. Then, at the set flow rate, the pressure



Fig. 1 Schematic representation of PLE experiment apparatus;
(1) ethanol solvent, (2) HPLC pump, (3) heating element, (4) solvent pre-heating section, (5) ½' extractor tube, (6) pressure gauge,
(7) hand-regulated valve, (8) sample vial

regulation was carried out manually and the isothermal conditions were kept by heated water bath. The preheating of the solvent was carried out in the same bath by submerging 2 m of the 1/16' capillary.

The total sampling time for the runs were 5 and 20 minute with 1 and 5 minute sampling intervals, respectively. The weight of each sample were measured before and after evaporation using a BiotageTM TurboVap LV stripper at 318 K with compressed air until completely dry  $(\dot{V}_{str} = 3.5 \text{ mL/min})$ . Samples were collected in sampling bottles and stored in a refrigator until analysis. After the extraction, the solid material was removed from the extractor and dried on air.

#### 2.2.2 Liquid-Liquid Extraction (LLE)

A hexane-methanol-water system was used in this series of measurements. The experimental plan can be seen in Fig. 2 [33]. This measurement aims to evaluate the effect of the composition on the CBD distribution ratio of the winterized natural hemp extracts. The five initial molar compositions can be seen in Table 1.

The basis of measurements was the combined dry extracts of all 20-minute PLE experiments. After dissolving the dry extract in ethanol, the liquid was cooled to 273 K for an hour, then the precipitated waxes of the cold liquid were removed by filtration (winterization). After that, the bulk solution was divided into five equal parts and then stripped dry at 318 K by the Biotage<sup>™</sup> TurboVap LV. The separated dry materials were weighted. The five dry material samples were dissolved in the five initial liquid-liquid mixture. Ultrasound was employed to enhance the dissolution of the heavier components.

In each step, the samples were mixed thoroughly for 10 minutes then submerged in a water bath set at 298 K for 1 h. After reaching equilibrium and phase settling a minimal (approximately) 0.5–1 mL sample was taken



Fig. 2 LLE experimental schematic; ★: initial composition,
→: represents the direction of methanol increase in each run; dashes curve: phase boundary at 298.15 K reported: [33]

Table 1 Initial molar composition of the liquid-liquid extraction runs

	$m_{\text{initial liquid}} = 250$	$m_{\text{initial liquid}} = 250 \text{ g}; m_{\text{dissolved dry mat.}} = 0.606 \pm 0.045 \text{ g}$		
Code	$x_{_{ m MeOH}}$	$x_{_{ m Hexane}}$	$x_{_{ m H_2O}}$	
1	0.1145	0.2511	0.6344	
2	0.1402	0.3688	0.4910	
3	0.1646	0.4741	0.3613	
4	0.1815	0.5904	0.2281	
5	0.2087	0.6788	0.1125	

from each phase. It was weighed, then stored in a refrigerator until analysis. Each new measurement point was achieved by adding to each system a known amount of methanol repeatedly.

At the last measurement point with the highest methanol content, a temperature dependence study was conducted. The samples were additionally kept at 323 K (water bath) and 278 K (refrigerator) for 2 and 12 h, respectively, and sampled in the same manner at both temperatures.

# 2.2.3 High-Performance Liquid Chromatography (HPLC) method: CBD analysis

After stripping the samples of the PLE experiments, the weighted dry material was dissolved in methanol until completely dissolved. An ultrasonic bath was used for approx. 10 minutes to guarantee the total dissolution and homogenization. A probe of volume around of 1-2 mL from the solution was filtered with a 0.02 µm syringe filter into a clean vial, and an amount of 100 µL of the filtrate was introduced to a clean vial and further diluted with 1.5 mL of methanol.

In the case of the LLE experiments, approximately 1 mL sample was taken from both phases, then weighted. The hexane-rich phase was vacuum distilled at 313 K, to 125 Pa. The water-rich phase was diluted with methanol to 20-times volume, then evaporated with the BiotageTM TurboVap LV. The dry material of both phases was redissolved with 300  $\mu$ L methanol and stored in a vial in a freezer (at 255 K) until analysis. The concentration of these samples varied in a wide range. Therefore, initially, 10  $\mu$ L was analyzed and after the results, the dilution ratio –by evaporation and redissolution– was decreased if the concentration was out of calibration range.

Jasco LG-980-02 Ternary Gradient Unit was providing gradient mixing. Jasco PU-1580 Intelligent HPLC pump was used to provide a constant flow rate with an upper-pressure limit of 25 MPa connected to a Jasco AS-2057 plus Intelligent Sampler. 10  $\mu$ L samples were injected (aside from some LLE samples). The components were separated on a 3.9 × 150 mm Waters Symmetry<sup>®</sup> C18 column with 5  $\mu$ m particle size, kept at 303 K. For compound detection a Jasco MD-910 (Multiwavelength Detector) photo diode array detector was used. For mobile phase a solvent mixture was used in gradient elution mode, the gradient profile is presented below, in the Table 2.

For quantitation, the CBD concentration had been calibrated with the dilution series of Cerilliant<sup>®</sup> 1 mg/mL CBD standard (product ID: C-045-1ML). The retention time of CBD was 6.5 minutes. Two calibration intervals had been determined. The detection was performed at the wavelengths of  $\lambda = 215$  nm 0.0123–0.111 mg/mL and at  $\lambda = 230$  nm, 0.111–1 mg/mL ranges. The coefficient of determination ( $R^2$ ) of the calibration lines were 0.9959 and 0.9997 from 3 and 4 measurement points, respectively.

#### 2.3 Data analysis

In the PLE experiments the calculation of results were the following:

$$Y_n = \left(\sum_{i=1}^n m_i\right) / m_{\rm dry \ mat.} \tag{1}$$

$$f_n = \left(\sum_{i=1}^n m_{i,\text{solvent}}\right) / m_{\text{dry mat.}}$$
(2)

wherein Eq. (1)  $Y_n$  is the yield [w/w%] at measurement point *n*;  $m_i$  is the mass of collected dry sample at measurement point *i* [g],  $m_{dry mat.}$  is the mass of the dry material filled in the extractor column initially [g], and in Eq. (2)

Table 2 Gradient profile of the HPLC method				
	$\dot{V}_{\text{total}} = 1 \frac{\text{mL}}{\text{min}}$			
Time [min]	[%]a	[%] <sup>b</sup>		
0	0	100		
1	0	100		
4	80	20		
7	80	20		
9	20	80		
11	0	100		

<sup>a</sup> 1:3 V/V mixture of a 25 mM ammoniumacetate aqueous solution with pH 4.7 (set with aceticacid) and Emplura<sup>®</sup> methanol, respectively;

<sup>b</sup> Emplura<sup>®</sup> methanol

*f* is the feed ratio [-] serving as a time-like variable;  $m_{i,\text{solvent}}$  is the used amount of solvent between measurement point *i* and *i*-1 [g].

The modified Brunner equation [34] is applied for the evaluation of the yield curves, defined as:

$$Y = x_o \times \left(1 - e^{-k \times f}\right),\tag{3}$$

where Y is the extraction yield [%];  $x_o$  is the total retrievable content of the target component(s) in the same dimension as yield; k is mass transfer-like coefficient [-], f is the feed ratio.

The regression of the Brunner equation was carried out by the optimization of both parameters  $x_o$ , k for each dataset. The least-squares method was applied to minimize the error, defined as:

$$\operatorname{Min}\left(\operatorname{Error}^{2}\right) = \sum \left(Y_{f_{n}}^{m} - Y_{f_{n}}^{\prime Br}\right)^{2},\tag{4}$$

where  $Y_{f_n}^m$  [%] is the measured yield at feed ratio *n*;  $Y_{f_n}^{Br}$  is the fitted Brunner equation at a feed ratio *n*.

The regressed  $x_o$ , k values were further studied with Statistica 13 (TIBCO Software. Inc., Palo Alto, CA) to evaluate the relation between the parameters and the independent variables of (P, T).

In the LLE experiments, the distribution ratio is defined as

$$K_D = \frac{C(\text{organic})}{C(\text{aqueous})},\tag{5}$$

where  $K_D$  [-] is the distribution ratio; *C*(organic) is the concentration of the studied component in the organic phase; *C*(aqueous) is the concentration of the same component in the aqueous phase. The concentration was given in mass concentration. Molar concentration cannot be used due to the complexity of the plant extracts.

#### **3** Results and discussion

### 3.1 Intensified PLE of hemp extraction

Two sets of total sampling time, 20 and 5 minutes, with 5 and 1 minute continuouse sampling was carried out according to a randomized three-level factorial design with pressure and temperature variables at 8–10–12 MPa and 323–333–343 K to investigate the effect of the parameters on the total- and CBD yields and to study the technical kinetics of the mass transport in a semi-continuous operation. Three central-point repetitions were included to further validate the results.

There are several mathematical descriptions of extraction processes based on different pore types and numerous assumptions [32–37]. The complexity, mainly the number of fitting parameters and coefficients, varies greatly in different models. One of the common mathematical descriptions of the semi-continuous solid-liquid extraction is based on the modified Brunner equation, see Eq. (3). The two parameters give information about both the total yield and the overall mass transfer.

In this study regression of the modified Brunner equation was carried out by the optimization of both parameters  $x_o$ , k for the results. The obtained values were further correlated with the independent variables, P and T.

#### 3.1.1 Yield curves and regression analysis

Considering the literature of batch PLE of hemp threshing residue experiments (extraction times [32]: 10–100 min; [31]: 45 min) 20 minute total sampling with 5 minute continuous sample collection was deemed fit to record the early stages of the extraction. The average errors of fitting by Brunner equation were 0.22 % and 0.01 % for the total- and CBD yield curves, respectively. However, the curves showed that in all cases at least 70 % of the yield was extracted in the first 5 minute period, see Fig. 3. Therefore, both total- and sampling time was further decreased to study the mass transport more accurately.

In the case of 1 minute continuous sampling up to 5 minutes, the average errors of fitting by Brunner Eq. were 0.60 % and 0.18 % for total- and CBD yields, respectively.

An example of the yield curves can be seen on Fig. 3. Both, total and CBD extraction yield curves are appropriately described with Eq. (3). Despite the good fitting results, both multiple- and response surface regression yielded no correlation with the independent variables when correlated with the fitted  $x_o$ , k values in Eq. (3) of all experiments (with a probability < 0.05). Most likely the selected pressure and temperature ranges were too narrow to determine any tendencies.



Fig. 3 Experimental data and fitted curves of PLE experiment; continuous lines: total yield fitted by Eq. (3), dotted line: CBD yield fitted by Eq. (3)

The highest CBD content can be achieved at 12 MPa, 343 K, and 2.7 feed ratio (approx. 15 min extraction), seen on Fig. 3. Comparing the best result with the one obtained from a previous study conducted by our SFE research group using the same plant material and carried out  $scCO_2$  extraction with 10 w/w% of ethanol co-solvent ( $scCO_2EtOH$ ) [25], we found the following: in case of PLE with ethanol, the operation time and solvent mass consumption have been decreased 20 and 31-fold, respectively. However, by fast and efficient PLE extraction the maximum CBD yield was 5.1 g CBD/g dry material, significantly lower than in the case of the co-solvent assisted supercritical fluid extraction (6.98 g CBD/g dry material). The CBD concentration of the PLE extract was also lower, 6.3 w/w% compared to 10.5 wt% obtained by scCO<sub>2</sub>EtOH.

The yield difference is most likely the result of the vast difference in solvent consumption, but it can be also explained by the easier penetration of the supercritical carbon dioxide into the solid matrix. The purity difference can be explained with the polarity difference of the two solvents. The lower CBD concentration of the PLE extracts is in agreement with the expectations. Ethanol dissolves various components from the plant material, while a carbon dioxide-based solvent mixture has a better selectivity towards the semi-polar CBD.

This novel semi-continuous PLE extraction results complete extraction with enhanced productivity with shorter extraction time and lower liquid-to-solid ratio (3 for semi-continuous PLE, 3.3-5 for the batch PLE [32]).

#### 3.1.2 Concentration profile of PLE

If the concentration of the solution obtained during the extraction was plotted against the feed ratio (or time) an exponential correlation was observed. In reality, the concentration of the liquid leaving the extraction column was not known because of the sampling method chosen. The measured values were an average concentration in a time interval. Therefore, plotting the logarithm of the concentration to the arithmetic average of the feed ratio was chosen. The results can be seen in Fig. 4 [25].

The plot shows that both the total extract and CBD concentrations decline rapidly in the early stage (up to feed ratio  $\approx 1-1.5$ ). The components on the surface of the plant material were rapidly dissolved and transported to the bulk. Then after the transition phase, the solid-diffusion control started. It was more distinct for the extract concentration profile.

Interestingly, if the results of the  $scCO_2$ -EtOH [25] were compared, at first, no similarity could be observed. However, when the consumed CO<sub>2</sub> was excluded from the



Fig. 4 Logarithmic concentration profiles of all PLE experiments and scCO<sub>2</sub>-EtOH [25] – with exclusion of CO<sub>2</sub> from the feed ratio;
(a) extract concentration profile, (b) CBD concentration profile; grey dashed lines just guide the eye

feed ratio calculations and only the 10 w/w% EtOH was considered as a solvent, a unique phenomenon was observed as it can be seen on Fig. 4 (blue dots). Both total extract- and CBD concentration curves of this so-called pseudo-concentration profiles of the semi-continuous supercritical extraction match the PLE profiles. Probably, the mass-transfer from solid to the liquid of the soluble components is highly enhanced by the ethanol. This phenomenon could also explain the more than 30-fold intensification of solvent mass consumption since the main factor was the ethanol.

#### 3.2 Results of LLE: distribution ratio results

After the plant material extraction, the purity of the extracts was typically not suitable for direct application in the cosmetic, pharmaceutical, or pharma industries. Bioactive components are typically heat sensitive, thus Liquid-Liquid Extraction is a common refining method. The distribution ratio (defined by Eq. (5)) is usually up to the experimental determination in all newly charted systems.

Five different compositions of hexane-methanol-water liquid-liquid equilibrium were created to study the distribution ratio of the winterized combined extracts from the PLE experiments with a 20 minute total sampling time. A fixed hexane-water ratio was used in each run and only the methanol content was further increased four times, without entering the single-phase region. A minimal quantity of samples (0.5–1 mL) were taken from the bulk after equilibration.

Before evaluation, the concentration profile was verified. Constant CBD concentration was not observed in any phase that means, that the solubility limit was not reached. The determined distribution coefficients are presented in Fig. 5.

High methanol dependency of the distribution coefficient can be observed. Increasing the methanol content facilitates the migration of CBD from the hexane-rich phase into the water-rich phase. This is most likely caused by the dual polar-apolar property of methanol thereby promoting the solution of the more apolar CBD in the waterrich phase. Advantageous property of the system is that by simply changing the methanol content, the distribution ratio crosses the  $K_D = 1$  threshold. From an operation perspective, this allows the possibility of a simple back extraction step which can be feasible just by fine-tuning the methanol content between multiple extraction steps.

To further investigate the results a temperature sensitivity study was conducted at the last measurement points (highest methanol content). The results can be seen on Fig. 6.

On the one hand, small temperature ( $\approx 1$  K) inhomogeneity throughout the study most likely does not seem to



**Fig. 5** Distribution coefficient as plotted against the solute-free liquid composition (H<sub>2</sub>O axis unmarked for better visibility); for measurement codes: see Table 1



Fig. 6 Temperature dependence study of all samples at the highest methanol content

produce considerable errors in the results, except for experiment with code 1 (see Table 1). In this case, the distribution ratio slightly decreases by the temperature lowering.

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# **4** Conclusion

In the studied T and P intervals the extraction kinetics of semi-continuous pressurized liquid extraction of hemp threshing residue is appropriately described by the modified Brunner equation (see Eq. (3) for both total- and CBD yield curves). The fitting errors does not exceed 1 %. The fitting parameters of Eq. (3) were further regressed to the independent variables P and T. Neither the extraction yield or rate was influenced by the variables, showing that the semi-continuous PLE with ethanol was a highly robust and efficient extraction method for the hemp treshing residues.

Compared to a previous ethanol and carbon dioxide mixture extraction study of the the same material, intensification was achieved by PLE with pure ethanol solvent. Both, solvent mass consumption and the operation time were decreased more than an order of magnitude in case of PLE. The evaluation of the concentration profiles showed that ethanol is highly facilitating the mass-transfer of all solutes.

The winterized dry extracts were further studied in a methanol-hexane-water system. The results show that the distribution ratio is highly dependent on the methanol content. The ratio equals 1 threshold is crossed which suggests a good back-extraction opportunity after a multistep forward extraction-based purification.

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