

In-situ measurements in Overconsolidated Clay: Earth Pressure at rest

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Abstract

The study is about the general genesis process of overconsolidated soils, as well as the effects of the overconsolidated ratio to structures. It will demonstrate the possible methods for the determination of the values of overconsolidated ratio and of earth pressure at rest; further, the processing of measurement results, through which the values of OCR (Overconsolidated ratio) and of λ_0 (Earth pressure at rest) in the Kiscelli Clay Marl have been determined.

Keywords

Coefficient of the earth pressure at rest · Overconsolidated ratio · Earth pressure cell · Borehole cell · Selfboring pressuremeter

1 Introduction

The need to utilise underground spaces was growing parallelly to fast expansion of large cities in the previous century, the growth-rate of which is further increasing these days. Building in underground spaces is supposed to be handled together with wider and wider exploration of soils and rock layers. The behaviour of overconsolidated soils is being explored and investigated globally, because significant horizontal stresses emerging in overconsolidated soil- and rock-strata give rise to unproportionally high horizontal loads to structures [2].

In the process of the investigations the objective was to determine the natural horizontal and vertical stresses at rest in the Kiscelli Clay Marl layer.

The effective stress or the stress condition at rest means a stress space free from human intervention, both in the rock- and in the soil-mechanical field. There are conditions used by both the soil- and rock-mechanics for the sake of simplification. These are for instance the homogeneity, the isotropicity and the elasticity of rock masses. The primary stress condition is the result of the dead-weight loads of rocks or soils but it can be changed by tectonic activities, desiccation or other physical influences. The determination of the coefficient of the earth pressure at rest differs significantly in the area of the classical soil-mechanics and in that of the classical rock-mechanics, which is demonstrated by Fig. 1. [1][3] The classical soil-mechanics uses the Jaky's formula to calculate the K_0 , which is the $K_0 = 1 - \sin \phi$. The coefficient of the earth pressure at rest is calculated by ν (angle of internal friction).

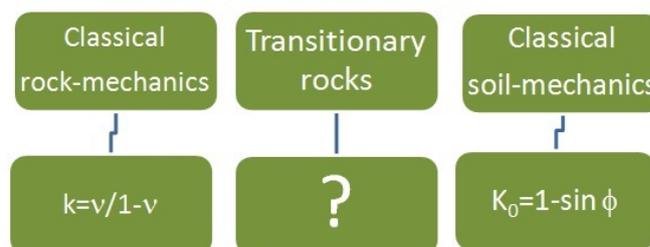


Fig. 1. Coefficient of the earth pressure at rest

The classical rock- mechanics uses the ν - Poisson's number

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to calculate the coefficient of the earth pressure at rest. [4][16]

The laboratory tests are used for the soils and the rocks, the soil models are used for the soils [5] while the rock models are used for the rock masses. These models are not used for the transitional rocks.

The best method to determine horizontal and vertical stresses is the use of local, in-situ investigations because these measurements have the least disturbing effects on the original stress conditions of a soil layer under test. The behaviour of the soils is determined by CPTu which is one of the world-wide best-known in-situ measurements [6] but horizontal earth pressure can be determined in indirect way.

Three different in-site investigations have been performed in order to determine the overconsolidated ratio and the earth pressure at rest: measurement with an earth-pressure cell; measurement with a borehole cell; and a measurement with a selfboring pressuremeter.

2 Geological, geotechnical environment

2.1 Geological environment

The rock layer of Kiscelli Clay Marl can be found beneath the major part of Budapest. It is situated on or near to the surface in the Buda-side of the city over a considerable area.

The thickness of the rock layer varies between 50 and 500 meters, but at certain spots it can reach even 1000 meters.

Kiscelli Clay was formed in the Cenozoic era of geohistory in the Tertiary period within that era.

The clay marl was depositing in the Oligocene, in its middle period when the location of the continents started to reach their today known location. Regarding the fauna of that period mammals were occupying an increasing area.

The Kiscelli Clay Marl is a marine deposit from the Middle-Oligocene. It was settling down among normal salty-water conditions in the Tethys-sea, which is considered to be the ancestor of the Mediterranean Sea of today. [7]

2.2 Geotechnical environment

Kiscelli Clay can be considered to be founding strata of the Quaternary period. After a rapid glance over geohistory it can be stated that Kiscelli Clay, after having deposited in the Oligogenic phase of the Tertiary period, became heavily consolidated later, upon the effects of soil layers deposited over it. [14][15]

At the end of the Tertiary period of geohistory and in the Quaternary period the thick conglomerates lying over Kiscelli Clay underwent a significant erosion process. As a result of this major erosion vertical loads of Kiscelli Clay were removed and its upper layers became loose.

Kiscelli Clay cannot be considered as a homogenous layer: its vertical stratification must be taken into consideration both in the design and in the construction phase.

In general it can be broken down to three well-distinguishable zones: (Table 1.)

- **Weathered zone:** This zone of Kiscelli Clay completely lost its properties characteristic of transitional rocks during the process of losing its loads and now it is in a plastic or near-plastic condition.
- **Fissured zone:** The properties of the fissured zone are similar to those of the intact zone, no plasticity can be detected anymore. The fissures-textured rock bodies are in sound condition with high solidity.
- **Intact rock mass zone, beyond the impact of expansion:** the deeper layers of Kiscelli Clay were not exposed to the load-relief impacts of erosion, so this zone conserved the ancient soil-physical properties of clay. Obviously the highest load deposited over the clay layer ever before, together with the resulting maximum consolidation, have also been preserved in this zone. The impact of a formerly existing maximum load ever is called overconsolidation.

3 In-site investigations applied

3.1 Earth pressure cell

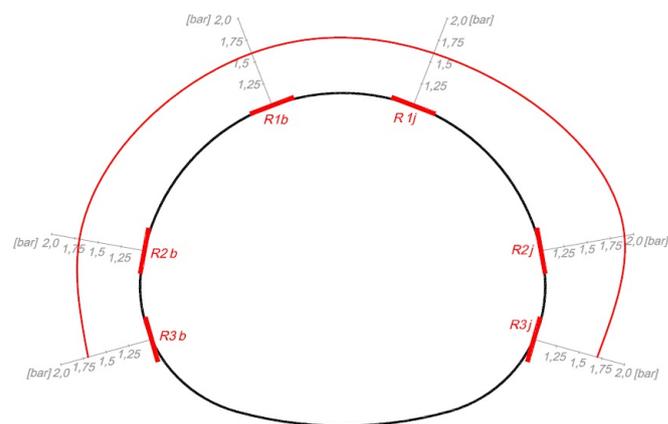


Fig. 2. Points at which the earth pressure cells are located, and their values

In the course of the investigations firstly earth pressure cells were used to determine the stresses to the tunnel being built in overconsolidated clay.[15] During the investigation radial cells made by company Glöttzl have been installed. (Fig. 2) These cells determined the value of the force exercised by the rock environment to the shotcrete wall. Six radial cells were installed in the system.

Processing the measurement results it was outlined that the value of horizontal and vertical stresses in the neighbourhood of the completed tunnel are nearly the same. [9]

3.2 Borehole cell

An earth pressure cell system installed into a borehole called Stress Monitoring System was installed during the investigations. Similarly to the pressure cells, the borehole cell (Fig. 3) is also made in Germany, by the firm Glöttzl. [11]

The name borehole cell refers to the place of the installation: the cell system is installed into a borehole. The borehole cell

Tab. 1. The soil-physical properties of Kiscelli Clay

Soil type According to Msz. 14043-2-1979	Bulk density of nat. state ρ_r [t/m ³]	Angle of internal friction φ [degree]	Cohesion c [kN/m ²]	Young modulus E_s [kN/m ²]	Consistency index I_c [-]	Void ratio e [-]
Wethered zone of Kiscelli Clay	2,1	20-23	50-100	7-10	> 1	0,4-0,68
Fissured zone of Kiscelli Clay	2,2	25-28	420	15-20	> 1, 2	0,32-0,4
Zone beyond the impact of expansion, Kiscelli Clay Marl	2,3	35-50	400-1000		> 1, 3	0,18-0,32

means a system of individual cells always compiled in accordance with individual needs. The system used here is made up of five cells, but obviously either more or less cells could also be combined together.

The purpose of the investigation was to determine the value of horizontal and vertical stresses in the overconsolidated Kiscelli Clay.



Fig. 3. Borehole cell

The borehole cell was installed in a stress-free area in a depth of 15 meters. The installation depth was selected with regard to the RQD indices. RQD index is the rock quality designation index which is a measure of the degree of jointing or fracture in a rock mass. The instrument was installed in the zone of the intact rock environment where the RQD is 70%.

The borehole cell system was installed on 19 May 2008 and keeps performing its measurement tasks until today after appropriate reconstruction and protection.

In the first 7 months there were two readings per day. Subsequently to the first 7-month period the number of readings reduced to one per day until the end of the first year. In the second year the number of readings could be further reduced to once a week, while after the first eighteen months following the installation of the instrument, the number of readings was decreased to once in two weeks.

3.3 Selfboring pressuremeter (SBP)



Fig. 4. Selfboring pressuremeter

During the research there was a chance to take part in investigations carried out with selfboring pressuremeter at several locations in Budapest [12, 13] The investigations were targeted at defining the overconsolidated ratio of Kiscelli Clay.

Since the measurement results could be used for scientific purposes the research group had the opportunity to investigate the Kiscelli Clay at various sites.

In the case of a selfboring pressuremeter the rock environment cannot expand after the borehole had been completed as it is continuously supported until the completion of the investigation process. This device allows us to determine the real, in-situ stresses in any cases.[11]

SBP is a special device combining the tooling required for boring and the pressuremeter instrument. The device is 1.2 m long with a diameter of 83 mm ending in a boring crown head.(Fig. 4)

The pressuremeter itself is a 0.5 meter long polyurethane membrane, protected with a stainless steel mantle. Inside the membrane there is a six-branch displacement meter measuring the displacements in the wall of the borehole. The six-branch displacement meter makes it possible to determine also

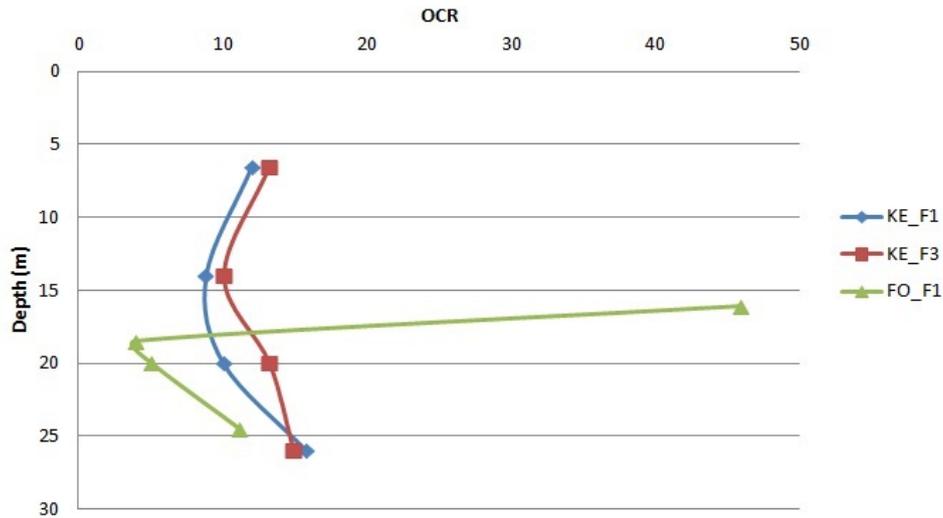


Fig. 5. OCR value versus depth value. KE_F1 ; KE_F3 - name of the measurements

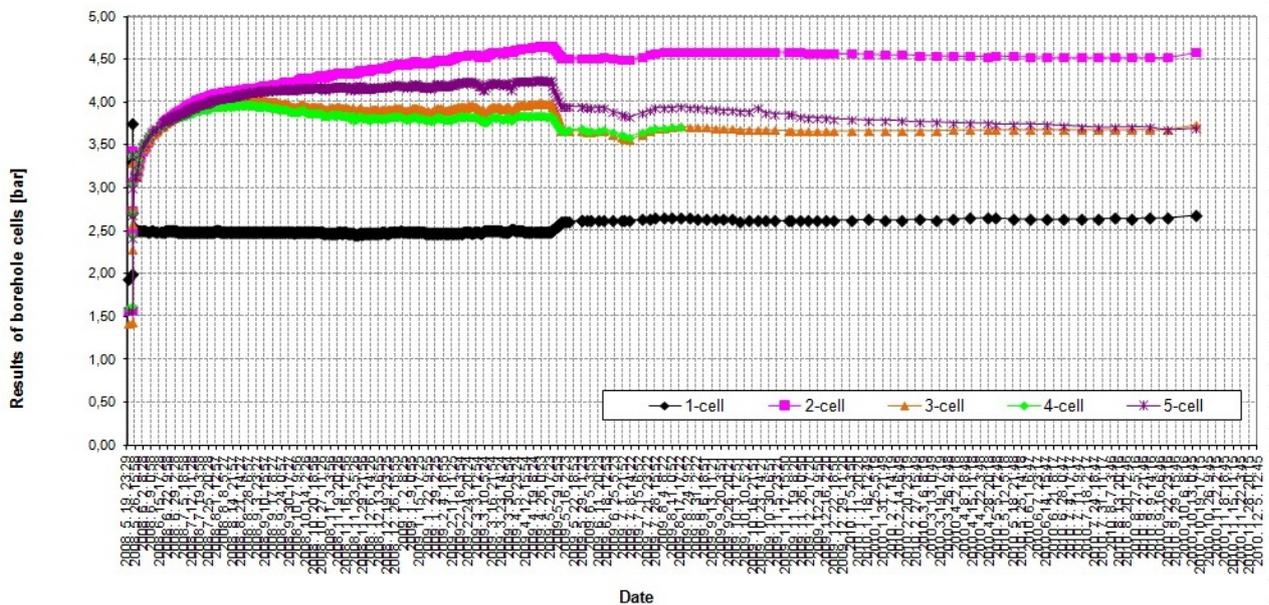


Fig. 6. Horizontal stress values versus depth values

the main direction of the horizontal stress, in addition to the size of stresses measured in the process. With the help of the horizontal stress instrument the research group was able to measure the total horizontal stress. If groundwater or strata-water is present this device measures not the horizontal stress accumulated in the layer but the horizontal stress of the layer and the stress of the water in the layer.[17] In order to enable the device to measure the effective stress of the soil/rock layer two cells are also installed outside the membrane to measure the pore-water pressure, the purpose of which is to determine the value of the neutral stress due to water pressure in the layer. If the total horizontal pressure and the neutral stress is known the effective horizontal stress can be determined.

The value of the OCR is determined by the values of the pure pressure and the critical state parameter.

$$\sigma_v^{max} = \frac{4 \times s_u}{M},$$

$$OCR = \frac{\sigma_v^{max}}{\sigma_v},$$

$$M = \frac{6 \times \sin(\varphi)}{3 - \sin(\varphi)},$$

s_u – pure pressure

M – critical state parameter

φ – angle of internal friction

In-situ measurements were carried out in the course of the investigations for more than two years to establish the overconsolidation ratio of the Kiscelli Clay caused by a preliminary loading, and the value of the resulting horizontal stress.

In order to determine the value of the coefficient of the earth pressure at rest we used the measurement results provided by

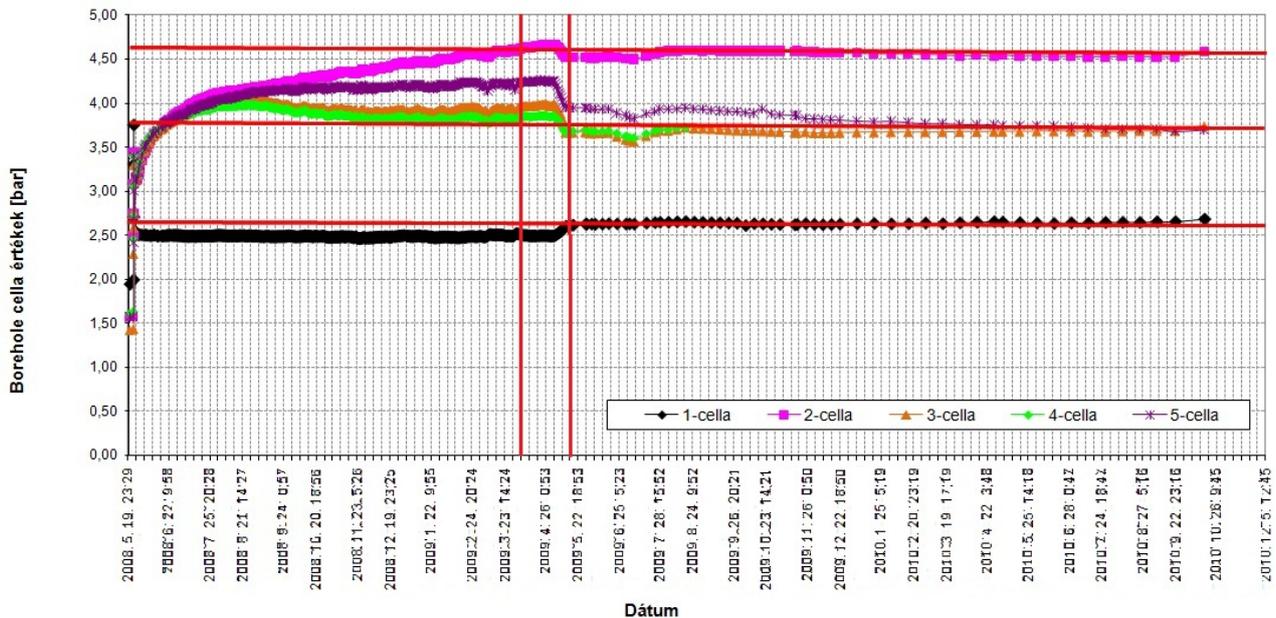


Fig. 7. Borehole-cell-measurement values in a time/pressure diagram. 1cell- vertical cell; 2cell,3cell,4cell,5cell-name of the horizontal earth pressure cells

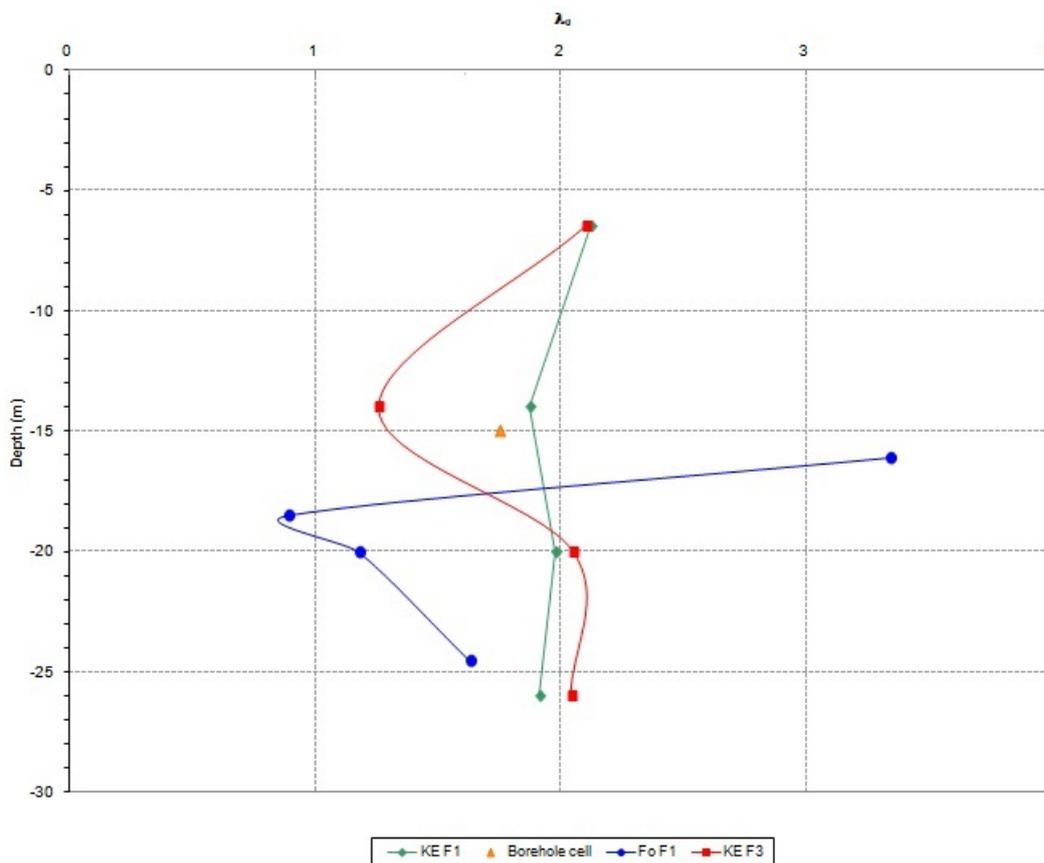


Fig. 8. Changes of the value of the coefficient of earth pressure at rest in the function of depth

the borehole cell and by the selfboring pressuremeter investigations. In the course of these investigations we determined not only the value of the coefficient of the earth pressure at rest but the research group investigated its evolution in depth too.

The value of the coefficient of the earth pressure at rest in Kiscelli Clay varies between 1.2 and 2.5 in the function of depth. (Fig. 8)

With the investigations performed to determine the overcon-

solidated ratio of Kiscelli Clay the research group established that the Kiscelli Clay, after its settling down, consolidated under the effect of a nearly 400-meter thick covering layer, and developed to its currently known condition. We were carrying out measurements through the installation of a borehole cell for more than two years, in order to establish the overconsolidated ratio. Then we processed the results of the measurements with a selfboring pressuremeter performed at three additional sites in

four different depths. Although I have used the values of two measurements to determine the OCR value. [10] The name of the boreholes are KE_F1 and KE_F3 where KE is the short code of Kelenföld station, place of the measurements and F1 and F3 are the names of the boreholes.(Fig. 5)

The Kiscelli Clay Marl is heavily overconsolidated, its overconsolidation ratio varies between 10 and 16 depending on depth.[7]

To determine the horizontal stress at rest the group used the results of the series of measurements of more than two years with the borehole cell as well as those of the selfboring pressuremeter investigations. The results of the borehole cell were depicted in a time/pressure graph. (Fig. 7). It was established that the values of the horizontal stress at rest were varying along an ellipse, and the maximum value of the stress in the intact rock mass zone of Kiscelli Clay is 4.62 bar.

As the result of the measurements with the selfboring pressuremeter we established that the value of the horizontal stress at rest varied between 270 and 1100 kPa depending on depth. (Fig. 6)

4 Conclusions

It can be established through the investigations that the method applied by classical soil mechanics and classical rock mechanics for the determination of the value of earth pressure at rest cannot be applied in the case of overconsolidated soils. In those situations where the stress values at rest for an overconsolidated soil must be determined, not even approaching calculations are recommended with the application of the rules of classical soil mechanics or classical rock mechanics.

The most accurate results for the determination of primary stresses are provided by in-site investigations. From among the scale of in-site investigations the measurements recommended for use are where the rock environment to be tested cannot expand.

In the course of the research work we demonstrated that the Kiscelli Clay is heavily overconsolidated and consequently the value of the horizontal stress is 1.5 to 2 times higher than the value of the vertical stress.

This result highly influences the static force impacts of the structures that are going to be built in the intact zone of Kiscelli Clay.

References

- 1 **Terzaghi V K**, *Theoretical Soil Mechanics*, John Wiley and Sons Inc., New York, 1943.
- 2 **Sivakumar V, Navaneethan T, Hughes D, Gallagher G**, *An assessment of the earth pressure coefficient in overconsolidated clays*, *Geotechnique* **59** (2009), no. 10, 825–838, DOI 10.1680/geot.8.P.033.
- 3 **Jáky J**, *New theory of earth pressure-Pressure of silos*, 2nd International Conference on Soil Mechanics and Foundation Engineering (Rotterdam, Holland).
- 4 **Széchy K**, *The art of Tunneling*, Tankönyvkiadó, Budapest, 1961.

- 5 **Varga G**, *Some geotechnical aspects of bioreactor landfills*, *Periodica Polytechnica Civil Engineering* **55** (2011), no. 1, 39–44, DOI 10.3311/pp.ci.2011-1.05.
- 6 **Mahler A, Szendefy J**, *Estimation of CPT resistance based on DPH results*, *Periodica Polytechnica Civil Engineering* **53** (2009), no. 2, 101–106, DOI 10.3311/pp.ci.2009-2.06.
- 7 **Kalman E**, *Geotechnical monitoring of the tunnel constructed in Kiscelli clay in Budapest*, The 2nd Symposium of Underground Excavations for Transportation (Istanbul, Turkey, November 15, 2007), Proceedings of the 2nd Symposium of Underground Excavations for Transport (TMMOB M.M.O.Y, ed.), 2007, pp. 509–516.
- 8 **Kalman E**, *Determination of the coefficient of the earth pressure at rest in overconsolidated clay*, 9th International Conference on Tunnel Construction and Underground Structures (Ljubljana, Slovenia, September 16, 2009), Proceedings of 9th International Conference on tunnel Construction and Underground Structures, 2009.
- 9 **Kalman E**, *Alagútbeli geotechnikai mérési tapasztalatok a Budapest 4. metro Bocskai úti állomás szellőző alagút építésénél*, *Geotechnikai Konferencia* (Ráckeve, Hungary, October 16, 2007).
- 10 **Sivakumar V, Doran I G, Graham J, Navaneethan T**, *Relationship between K_0 and overconsolidation ratio*, *Geotechnique* **52** (2002), no. 2, 225–230.
- 11 **Clark B G**, *The interpretation of self-boring pressuremeter tests to produce design parameters*, Blackie Academic and Professional an imprint of Chapman and Hall, Glasgow, 1993.
- 12 **Horváth T**, *Budapest Metro Line 4 Kelenföld Junction Station and Reversing Facility, Additional Site Investigation, Geotechnical Study 1 and 2*, Cambridge Institute and Geovil, 2008.
- 13 **Horváth T**, *Budapest Metro Line 4 Fovam ter Station, Additional Site Investigation, Geotechnical Study 1 and 2*, Cambridge Institute and Geovil, 2008.
- 14 **Horváth T**, *Expert opinion on the geotechnical, engineering geological and hydrogeological issues regarding the Kelenföld Junction Station, Geotechnical Study*, 2005.
- 15 **Horváth T**, *Expert opinion on the geotechnical, engineering geological and hydrogeological issues regarding the Bocskai Street Station, Geotechnical Study*, 2005.
- 16 **Hudson J A, Christiansson R**, *ISRM suggested methods for rock stress estimation- Part 4: Quality control of rock stress estimation*, *International Journal of Rock Mechanics and Mining Sciences* **40** (2003), 1021–1025, DOI 10.1016/j.ijrmms.2003.07.011.
- 17 **Yu H S, Collins I F**, *Analysis of self-boring pressuremeter tests in overconsolidated clays*, *Geotechnique* **48** (1998), no. 5, 689–693.