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RESEARCH ARTICLE

Stress Analysis of Segmental Tunnel Lining Using Artificial Neural Network

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Abstract

The paper describes an artificial neural network method (ANNM) to predict the stresses executed on segmental tunnel lining. An ANN using multi-layer perceptron (MLP) is developed. At first, database resulted from numerical analyses was prepared. This includes; depth of cover (H), horizontal to vertical stress ratio (K), thickness of segment (t), Young modulus of segment (E) and key segment position in each ring (θ) on the tunnel perimeter as input variables. Different types of stresses and extreme values of displacement have been considered as output parameters. Sensitivity analysis showed that the cover of the tunnel and key position are the most and less effective input variables on output parameters, respectively. Results for coefficient of determination (R^2) , variance accounted for (VAF), coefficient of efficiency (CE) and root mean squared error (RMSE) illustrates a high accuracy of the presented ANN model to predict the stress types and displacements of segmental tunnel lining.

Keywords

artificial neural network, tunnel, segment, lining, yield criterion

1 Introduction

Support lining of tunnels excavated by shield type of TBMs (Tunnel Boring Machine) is installed immediately after excavation of surrounding media. The support system of tunnel lining is composed of pre-casted reinforced concrete segments. Successive assembling of these concrete segments inside the TBM's shield, forms tunnel support rings. Design and construction of concrete segments are one of the most important steps in tunnel construction operation [1–4]. To simplify installing and assembling of ring erection operation, one segment is designed usually in trapezoidal shape which is smaller than the others and called key segment. Key segment will be installed at the end. Fig. 1 shows one assembled ring of concrete segments in segment manufacturing factory.



Fig. 1 An assembled concrete segmental ring, Segment factory, Tehran Metro-Line 4 [5]

Generally, design methods of tunnel lining can be classified in 3 different approaches: Analytical, Experimental and Numerical methods.

Analytical methods have been developed from the start of the tunnel support design history up to now [6-16]. Some of these analytical methods are restricted either to only elastic behaviour of tunnel lining and soil material or only to shallow tunnel conditions. Some others, taking into account few simple

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assumptions with reduced stiffness of segmental ring without consideration of longitudinal joints in reality. And some others do not consider smaller key segment size with respect to other segments in tunnel support ring and consider all of them with the same size.

Nowadays some attempts in design and analysis of segmental tunnel lining are carried out based on the laboratorial studies [17–23]. Other methods are often verified by experimental methods. The experimental methods are much more useful than analytical and numerical methods, but these methods are mostly time consuming and expensive.

Numerical methods have been developed widely in recent decades [24–29]. Numerical methods are often time consuming and need more detailed input data that could be unknown during analysis. Also these methods often need to advanced computer systems for analyzing. The results of numerical methods must be verified by either experimental, analytical methods or by in-situ monitoring results.

In recent years, to overcome with all above mentioned difficulties, new methods such as Fuzzy systems and Artificial Neural Network (ANN) models have been used as a prediction tool for analysis of complicated problems. ANN approach has been used widely in geotechnical and geomechanical engineering problems [30–42]. Due to above mentioned defects of numerical, experimental and analytical methods in design of segmental tunnel lining, application of ANN methods seems to be a new alternative solution as prediction tools.

Prediction of yield stresses and extreme values of tunnel lining ring displacement using ANN was not studied in detail as of yet. In this study, ANN method has been used to predict yield stresses and displacement of segmental tunnel lining ring based on the results obtained from numerical method. Sensitivity analysis of input variables performed to determine their effects on output results. Finally the performance of the model was evaluated by means of root mean squared error (RMSE) in percent (%), coefficient of determination (R^2), proportion of variance explained (PVE) or variance accounted for (VAF) in percent (%), and coefficient of efficiency (CE) indices.

2 Yield criteria

There are two most commonly used criteria in strength of materials: Von Mises and Tresca criteria. According to Von Mises yield criterion, material starts to yield once the second deviatoric stress invariant approaches to a critical value. In this criterion, Von Mises stress denoted by σ_v and when reaches to yield strength of material known as σ_y , it begins to yield. Von Mises stress can be calculated from Eq. (1) [43]:

$$\sigma_{v}^{2} = 0.5 \times \left[\left(\sigma_{11} - \sigma_{22} \right)^{2} + \left(\sigma_{22} - \sigma_{33} \right)^{2} + \left(\sigma_{33} - \sigma_{11} \right)^{2} + 6 \left(\sigma_{23}^{2} + \sigma_{31}^{2} + \sigma_{12}^{2} \right) \right]$$
(1)

Where:

 $\sigma_{\rm w}$: Von Mises stress;

 σ_{ii} : Components of stress tensor.

Also, according to Tresca yield criterion, material starts to yield once maximum absolute value of shear stress in a material reaches to a critical value. It must be noticed that stress values of two yield criteria are calculated based on principal stress components. Comparison between both yield criteria is shown in Fig. 2.



Fig. 2 Von Mises and Tresca yield surfaces [44]

3 Artificial neural network and multilayer perceptron

Artificial neural networks are composed of many data processing units called neurons. The aim of model is to simulate the act of human brain nature based on trial and error method using neurons [34, 45]. There are a large number of interconnections among the neurons in an ANN model. Generally speaking, a neural network model mostly composed of three layers in series, named: input layer, hidden layer(s) and output layer, respectively. Schematic view of a usual ANN is shown in Fig. 3. Hidden layer(s) is important layer of each neural network because the major calculation process is performed in this layer. Neurons on each layer are connected to the neurons of neighbouring layers with a coefficient named weight (w). Transform functions are used to transform the weighted sum of all input signals towards a neuron and calculate the output response of neuron. TANSIG and LOGSIG are two efficient non-liner sigmoid transform functions used in neural networks [37]. The output of an input layer is used as input for the hidden layer(s) and the same rule is applicable between hidden layer(s) and output layer, respectively. Optimum number of hidden layers and neurons are calculated based on trial and error rule and goal error value [34].



Fig. 3 Schematic view of a usual ANN [45]

At first, artificial neural network is trained by input data. Then tested and verified by other different input data. In training process, inputs are entered and outputs values are determined. Then error between predicted and real values is calculated. Based on these error values, the weights are adjusted by starting from the output layer towards the input layer. This process is known as Back Propagation (BP) algorithm. Back propagation algorithms are powerful tools for prediction models [45].

Perceptron neural net model proposed by Rosenblatt [46]. Then multiple layer perceptron neural network model was improved and proposed by Rumelhart [47]. In this model, the input layer normalizes input data values. This kind of data preparation and normalization, improves the network performances due to more homogeneous distribution of normalized data as shown in Fig. 4. This kind of normalization has been used by many researches [42, 46–49].

Except the input neurons, each neuron has a non-linear activation function. Multi-layer perceptron (MLP) is a modification of the standard linear perceptron, which can separate data that are not linearly separable [50].



Fig. 4 Effect of data normalization on the homogeneity distribution [49]

4 Numerical modelling

To use an artificial neural network as prediction tool, at first should prepare comprehensive input data. Using this database, neural net will be trained, tested and validated. To do this, in this study the results obtained from finite element program (ABAQUS, [51]) were used as database. In designed numerical models, the support system of segmental tunnel lining is supposed to be one ring with 5 + 1 segments. The engineering and

geometrical properties of concrete segments are summarized in Table 1. Five concrete segments (named A2–A6) are almost similar to each other from geometrical point of view except key segment. To reduce the total time of numerical operation, soil elements are neglected in numerical model. Beamspring method was used to model the tunnel lining structure [1, 2]. In this method the effects of soil body on tunnel lining and interaction between contact surfaces were simulated by means of tangential and radial springs. Tangential springs were neglected due to their negligible effects in comparison with radial springs. Stiffness of soil radial springs is calculated using Eq. (2), [52]:

$$K = \frac{A.E}{R.(1+\nu)} \tag{2}$$

Where:

K = stiffness of radial spring;

E = Y oung modulus of soil;

v = poison's ratio of soil;

R = tunnel radius; and

A = effective area of tunnel lining that is subjected to implied force from the soil, and calculated by Eq. (3):

$$A = R\theta.b \tag{3}$$

Where:

 θ = radial angle between two successive radial springs, and b = effective area of each spring in tunnel longitudinal direction.

Figs. 5a–b show the non-perspective and perspective view of tunnel lining under soil imposed radial springs.

Table 1 Engineering and geometrical properties of concrete segments

	Engineering properties			Geometrical properties		
Segment No.	E*	v**	ρ ***	t ****	Central angle(°)	
A1(key segment)	25	0.15	2250	20	30	
A2-A6	25	0.15	2350	30	66	

*Young modulus (GPa), **poisson ratio, *** density (kg/m³), **** thickness(cm)

3D solid elements type was used to model the concrete segments. After assembling concrete segments to each other, plane strain condition was applied to the model. In this attempt, it is assumed that origin of angle in model plane is located at tunnel crown (Fig. 6a). Joints between two neighbouring segments named longitudinal joints .Fig. 6b shows longitudinal joints of assembled segments in a ring and the position of key segment at $\theta = 90^\circ$. The assembled ring presents the tunnel lining support system. Hard contact was supposed for six concrete to concrete contact surfaces between concrete segments with frictional penalty coefficient of 0.4.



Fig. 5 Tunnel lining under soil imposed radial springs in radial direction





(a) Extreme Values of Von Mises Stresses (N/m^2)



(b) Extreme Values of Tresca Stresses (N/m^2)



(c) Maximum Value of maximum principal Stress (N/m^2)



(d) Extreme values of ring displacement (m)



5 Data collection and preparation for artificial neural network

The numerical model at first was solved for t = 30 cm, overburden H = 5m, K = 0.5 (horizontal to vertical stress ratio), E = 25 Gpa and $\theta = 0^{\circ}$. Then t, H, K and E values were kept constant and θ value changed 30°, 60°, 90°, 120°, 150° and 180° respectively. To prepare database, for each value of input variables, values of other input variables were changed according to values mentioned in Table 2. Table 2 shows the times of changes of each input variable and their magnitudes. Key positions at 210°, 240°, 270°, 300° and 330° at tunnel periphery were neglected due to the axisymmetric shape of tunnel lining ring. Finally 252 numerical models were analyzed. Some randomly selected input data variables and resulted outputs are summarized in Table 3. Figs. 7a-d show the values resulted for Von Mises and Tresca stresses together with principal stresses and extreme values of ring displacements for t = 30 cm, H = 15 m, K = 0.5, E = 20 Gpa and $\theta = 0^{\circ}$.

Table 2 Different values for input variables

Different values of 5 Input Variables							
t (cm)	H(m)	Key Position(°)					
	5	0.5		0			
				30			
30			25	60			
	15	1.0		90			
				120			
40			35	150			
	25	1.5		180			

Number of total numerical models: 2*3*3*2*7=252.

6 Application of ANN

6.1 Data Normalization

To increase the processing and convergence rate during training process and to minimize the prediction error, raw data must normalized [53]. Before modelling commences, all data should be checked and any false data must be deleted. Then data should be normalized to bring all of the variables into proportion with one another. To normalize data, traditionally this means to fit the data within unity, so all data values will be in the range of 0 to 1.

Equation 4 is what should be used to implement a unitybased normalization [54]:

$$u_{Norm} = \frac{u - u_{\min}}{u_{\max} - u_{\min}}$$
(4)

Where:

u: any raw data u_{Norm} : normalized data u_{min} : minimum value of data

u_{max} : maximum value of data

6.2 Optimum architecture of MLP Model

Obtained data from numerical modelling were used to prepare the multi-layer perceptron model for prediction aim. In this study, data were divided into 3 parts: training data (70% of total data), testing data (20% of total data) and validation data (10% of total data). The optimum structure (number of hidden layers) and optimum number of neurons in hidden layers of neural network model could be determined based on trial and error rule.

At first, the optimum numbers of neurons were calculated based on RMSE values. Then, obtained optimum number of neurons were embedded on hidden layers of the model.

RMSE value was calculated according to Eq. (5):

$$RMSE = \sqrt{\frac{1}{N} \sum_{i=1}^{N} (\hat{u}_{k} - u_{k})^{2}}$$
(5)

Where:

RMSE = Root mean square error value;

 \hat{u}_{k} and u_{k} = the kth predicted and observed values of target, respectively; and

N = the number of observations for which the error has been computed

The obtained results are illustrated on Fig. 8. It can be seen that the minimum value of RMSE was obtained by 11 number of neurons. Also there are some relation to estimate number of neurons in hidden layers. These relations are presented in Table 4.

So, the obtained number of neurons for hidden layers by RMSE value is in accordance with Hecht-Nielsen (1987) and Kanellopoulas and Wilkinson (1997).

Table 3 Randomly selected raw data obtained from finite element method

No. P. No. No. No. No. No.		Input variables Output parameters												
1 0 5 0 3	No	t1	H^2	K	E ³	θ^4	MisesMax ⁵	MisesMin ⁶	TrescaMax ⁷	TrescaMin ⁸	MaxPrinMax ⁹	MinPrinMin ¹⁰	UMax ¹¹	UMin ¹²
1 1 1 2	1	30	5	0.5	20	0	3.003E+06	3.606E+05	3.269E+06	4.065E+05	8.101E+05	-2.896E+06	5.132E-03	2.151E-03
1 0 5 0	2	30	5	0.5	20	30	2 768E+06	3 356E+05	3 019E+06	3 801E+05	8 818E+05	-2.686E+06	5 211E-03	2.178E-03
4 5 6 5 6 5 6 5 7 5 6 5 7 5 6 5 7 5 6 5 7 5 6 5 7 5 6 5 7 5 6 5 7 5 6 5 7 5 6 5 7 5 6 5 7 5 6 7 7 5 6 7 7 6 7 <th7< th=""> 7 <th7< th=""> <th7< th=""></th7<></th7<></th7<>	3	30	5	0.5	20	60	3.099E+06	3.148E+05	3 381E+06	3.426E+05	9 302E+05	-2.957E+06	5.242E-03	2.189E-03
1 1	4	20	5	0.5	20	00	2.695E+06	2 422E+05	2.017E+06	2.5%E+05	9.302E+05	-2.937E+00	5.117E.02	2.167E-03
3 3 5 0 2 1 2 2 0 3 1 2 1	4	30	5	0.5	20	90	2.083E+06	3.432E+03	2.91/E+06	3.380E+03	8.313E+03	-2.010E+06	5.007E 02	2.162E-03
6 70 75 <th75< th=""> 75 75 75<td>5</td><td>30</td><td>2</td><td>0.5</td><td>20</td><td>120</td><td>2.9/3E+06</td><td>2.976E+05</td><td>3.248E+06</td><td>3.256E+05</td><td>8.148E+05</td><td>-2.833E+06</td><td>5.08/E-03</td><td>2.144E-03</td></th75<>	5	30	2	0.5	20	120	2.9/3E+06	2.976E+05	3.248E+06	3.256E+05	8.148E+05	-2.833E+06	5.08/E-03	2.144E-03
7 30 5 10 5 10 5 10 5 10 5 10 11	6	30	5	0.5	20	150	2.710E+06	2.738E+05	2.967E+06	3.147E+05	8.246E+05	-2.618E+06	5.175E-03	2.115E-03
8 9 5 0 3,500+100 3,700E+00 3,944+05 0,444+05 0,2454+06 2,455E+03 2,455	7	30	5	0.5	20	180	3.181E+06	3.433E+05	3.469E+06	3.861E+05	9.749E+05	-3.045E+06	5.285E-03	2.132E-03
9 9 5 30 31441:06 31441:06 71441:06 71441:06 71441:06 71441:06 71441:06 71441:06 71441:06 71441:06 7144:06 <td>8</td> <td>30</td> <td>5</td> <td>0.5</td> <td>35</td> <td>0</td> <td>3.389E+06</td> <td>3.500E+05</td> <td>3.708E+06</td> <td>3.944E+05</td> <td>9.477E+05</td> <td>-3.208E+06</td> <td>4.844E-03</td> <td>2.459E-03</td>	8	30	5	0.5	35	0	3.389E+06	3.500E+05	3.708E+06	3.944E+05	9.477E+05	-3.208E+06	4.844E-03	2.459E-03
10 5 6.5 5.5 6.0 2.4284-00 2.8284-00 3.0578-05 3.0674-05 2.4887-00 4.2284-00 4.2382-00 4.2488-00 4.2382-00 2.4887-00 4.2488-00 12 30 5 0.5 5.5 10 3.081-00 2.6481-00 2.2481-00 4.2481-00 2.4481-00 4.2481-00 14 30 5 0.5 5.5 10 3.081-00 3.181-00 3.5578-05 1.121-106 4.9481-03 2.4381-00 15 30 5 1 2.0 0.0 1.9481-00 4.3581-00 5.1081-05 2.4881-00 4.7381-00 4.9381-00 4.9381-00 6.9081-03 4.9381-00 10 5 1 2.0 10 1.4481-01 4.3381-00 5.7076-06 2.7381-00 4.9381-00 6.9081-03 5.8381-00 5.3881-00 5.7381-00 6.7381-00 5.8381-00 5.7381-00 6.7381-00 5.8381-00 5.7381-00 6.7381-00 5.7381-00 5.7381-00 5.7381-00 5.7381-00<	9	30	5	0.5	35	30	3.111E+06	3.369E+05	3.414E+06	3.746E+05	1.005E+06	-2.952E+06	4.909E-03	2.488E-03
11 20 5 90 2907-06 3486-00 37081-05 9.818-05 -2.8405-00 4.827E-03 2.4881-03 13 00 5 0.5 35 100 3322E-06 3.006-06 3.006+05 9.232E+06 3.082E+06 3.045+06 3.056+05 2.342E+06 4.3062-03 2.332E+06 4.066-03 2.432E+03 16 30 5 1 20 0.8 8.773E+06 4.308E+06 5.358E+05 2.348E+06 -5.332E+06 6.868E-03 2.332E+06 3.938E+03 3.858E+04 17 10 5 1 20 0.8 8.778E+06 4.351E+06 2.352E+06 3.932E+06 6.338E+04 6.338E+04 <th< td=""><td>10</td><td>30</td><td>5</td><td>0.5</td><td>35</td><td>60</td><td>3.495E+06</td><td>2.829E+05</td><td>3.832E+06</td><td>3.057E+05</td><td>1.066E+06</td><td>-3.274E+06</td><td>4.932E-03</td><td>2.498E-03</td></th<>	10	30	5	0.5	35	60	3.495E+06	2.829E+05	3.832E+06	3.057E+05	1.066E+06	-3.274E+06	4.932E-03	2.498E-03
12 30 5 30 </td <td>11</td> <td>30</td> <td>5</td> <td>0.5</td> <td>35</td> <td>90</td> <td>2.967E+06</td> <td>3.486E+05</td> <td>3.250E+06</td> <td>3.768E+05</td> <td>9.618E+05</td> <td>-2.840E+06</td> <td>4.827E-03</td> <td>2.468E-03</td>	11	30	5	0.5	35	90	2.967E+06	3.486E+05	3.250E+06	3.768E+05	9.618E+05	-2.840E+06	4.827E-03	2.468E-03
11 10 5 15 15 15 15 3081-06 3091-06 3091-06 3091-06 3031-06 4041-03 4231-03 15 30 5 1 20 0 8731-06 4501-06 5331-06 4501-06 -7332-06 4021-05 7332-06 16 30 5 1 20 0 1731-07 5331-06 4391-06 53981-06 23981-06 -7332-06 4391-07 4391-06 4391-07 4391-06 4391-07 4391-06 4391-07 4391-07 4391-06 4391-07 4391-06 4391-07<	12	30	5	0.5	35	120	3.322E+06	2.633E+05	3.646E+06	2.864E+05	9.523E+05	-3.111E+06	4.799E-03	2.454E-03
14 30 5 15 35 16 398766 3947676 5108769 1124766 -7.3128766 69461.03 7.338240 15 30 5 1 20 0 9.79444764 5.206640 8.9118760 2.338243 2.34847646 -6.7342466 6.64641.03 7.338240 17 30 5 1 20 0 7.7944764 4.548240 7.797660 4.797640 3.7982460 -7.3384766 6.6661.03 5.338143 10 5 1 20 10 7.777660 4.777660 3.7978766 3.7928760 7.334766 6.7337460 7.334766 6.737766 4.7374767 5.0878-05 3.9928766 7.3328-06 6.5081.03 1.41870 12 30 5 1 35 30 2.168470 1.038767 5.2387-05 3.99287-06 3.3387-06 6.3382.03 1.2487.03 1.2487.03 13 30 9 1.385 30 2.1484.03 2.3486.03 3.3387.0	13	30	5	0.5	35	150	3.081E+06	2.732E+05	3.390E+06	3.096E+05	9.500E+05	-2.912E+06	4.866E-03	2.423E-03
15 30 5 1 20 0 873E+64 4.59E+65 2.848E+60 2.746E+66 6.73E+66 6.673E+06 6.73E+06 6.73E+06 6.73E+06 6.73E+06 6.73E+06 7.83E+04 18 30 5 1 20 0 0.73E+06 4.53E+00 2.74E+06 2.84E+06 2.89E+06 6.73E+06 6.73E+03 5.48E+04 19 30 5 1 20 10 1.77E+07 2.52E+05 3.92E+06 7.38E+06 7.38E+06 5.02E+04 21 30 5 1 20 1.8 0.97E+06 4.24E+05 1.03E+07 4.89E+05 2.78E+06 7.38E+06 6.58E+03 3.108E+06 7.38E+06 6.38E+03 1.24E+04 23 30 5 1 35 10 1.02E+07 4.73E+05 3.02E+06 3.39E+06 6.39E+03 3.24E+04 24 30 5 1 35 10 1.04E+07 4.31E+07 3.08E+05 3.24E+06	14	30	5	0.5	35	180	3.599E+06	3.182E+05	3.945E+06	3.557E+05	1.124E+06	-3.382E+06	4.964E-03	2.437E-03
16 30 5 1 20 30 7 944E-06 5 20E-05 8 911E+06 5 938E+05 2.746E+06 4.734E+06 6.846E-03 7 393E-04 17 30 5 1 20 60 1.134E+07 4.331E+03 2.348E+06 4.738E+06 4.738E+06 5.849E+04 10 30 5 1 20 10 1.147E+07 5.297E+03 3.392E+06 6.7328E+06 7.7378E+06 6.138E+03 7.3078E+06 7.378E+06 6.138E+03 7.3078E+06 7.378E+06 7.378E+06 <td>15</td> <td>30</td> <td>5</td> <td>1</td> <td>20</td> <td>0</td> <td>8.973E+06</td> <td>4.509E+05</td> <td>1.015E+07</td> <td>5.100E+05</td> <td>2.848E+06</td> <td>-7.312E+06</td> <td>6.902E-03</td> <td>4.194E-04</td>	15	30	5	1	20	0	8.973E+06	4.509E+05	1.015E+07	5.100E+05	2.848E+06	-7.312E+06	6.902E-03	4.194E-04
1 1 2 60 1.342-00 4.351-00 1.232-00 4.351-00	16	30	5	1	20	30	7 944E+06	5 206E+05	8 911E+06	5 938E+05	2 746E+06	-6 734E+06	6 864E-03	7 393E-04
1 0 5 1 20 00 1711100 4.54E+00 1.271100 4.701100 3.901100 7.2891+00 6.2811+00 5.3054+01 19 30 5 1 20 120 1.1471+07 5.2951+05 1.3071+07 5.9051+00 7.3241+06 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 6.9811+00 7.3241+00 21 30 5 1 35 30 9.212+06 8.8811+00 6.3911+00 7.2341+00 6.3911+00 7.2341+00 23 30 5 1 35 10 9.212+00 7.8811+00 7.3311+00 6.3911+00 7.2341+00 24 30 5 1 35 10 9.212+104 1.3311+00 1.3311+00 1.2311+00 1.3311+00 1.2311+00 1.3311+00 1.2311+00 1.3311+00 1.2311+00	17	20	5	1	20	60	1.124E+07	4 351E±05	1 203E±07	4.781E+05	2.740E+00	-0.754E+00	6 759E 03	5 840E 04
18 90 5 1 20 90 0.05700 5.258-100 5.056-10 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 5.288-100 6.508-100 6.508-100 5.002-140 12 30 5 1 35 0 9.247-100 4.202-100 1.0481-07 5.288-105 3.188-104 6.538-103 7.238-104 6.538-103 7.238-104 6.538-103 7.238-104 6.538-103 7.238-104 6.538-103 7.238-104 6.538-103 7.238-104 6.538-103 7.238-104 6.538-103 7.238-104 6.538-103 7.238-104 6.538-103 7.238-104 6.548-103 7.017-103 7.238-104 6.548-103 7.017-103 7.238-104 6.548-103 7.017-103 7.238-104 6.548-103 7.017-103 7.238-104 6.548-103 7.017-103 7.238-104 6.548-103 7.017-103 7.238-104	10	20	5	1	20	00	9.702E+06	4.551E+05	0.776E+06	4.781E+05	2.804E+06	-8.995E+00	6.991E.02	5.649E-04
19 30 5 1 20 120 120 120 120 230 250 120 120 120 877-100 53022-100 53022-100 63022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 73022-100 <th7302-100< th=""> 73022-100 <th7302-100< th=""></th7302-100<></th7302-100<>	10	20	5	1	20	90	8.703E+00	4.343E+03	9.770E+00	4.970E+05	2.094E+00	-7.289E+00	0.881E-03	5.403E-04
20 30 5 1 20 150 87/RE+00 4.30E+04 4.30E+04 4.27/RE+00 4.20E+04 5.30E+04 7.32E+00 6.30E+03 5.00E+03 5.00E+03 7.32E+04 6.30E+03 7.32E+04 7.32E+04 7.32E+04 7.32E+04 7.32E+04 7.32E+04 7.32E+04 7.32E+04 7.32E+04 7.33E+04 6.31E+03 7.32E+04 7.33E+04 7.33	19	30	5	1	20	120	1.14/E+0/	5.259E+05	1.30/E+0/	5.905E+05	3.992E+06	-9.080E+06	6.969E-03	6.338E-04
21 30 5 1 20 180 9077E+06 4.42E+05 1.04EE+07 4.87E+05 2.885E+06 7.38E+06 6.720E+03 6.39E+03 7.22E+04 24 30 5 1 35 30 9.216E+06 5.048E+07 5.08E+05 3.108E+06 -7.38E+06 6.39E+03 7.22E+04 25 30 5 1 35 60 1.12E+07 4.293E+05 1.290E+107 4.570E+05 3.92E+06 8.891E+06 6.312E+03 9.874E+04 26 30 5 1 35 120 1.14H+07 4.971E+05 1.30E+07 5.162E+05 3.98E+06 -7.373E+06 6.446E+03 9.02E+04 28 30 5 1.5 20 0 1.234E+07 5.10E+05 1.69E+05 3.18E+06 -3.07E+06 6.446E+03 9.92E+04 30 5 1.5 20 0 1.244E+07 5.16E+06 1.41E+07 1.22E+06 4.06E+07 1.91E+02 2.144E+03 <	20	30	5	1	20	150	8.778E+06	4.737E+05	9.860E+06	4.880E+05	2.767E+06	-7.324E+06	6.608E-03	5.002E-04
22 30 5 1 35 0 9.247E+06 5.448E+07 4.897E+05 2.853E+06 7.582E+06 6.305E+03 7.282E+06 7.30E+06 6.34E+04 0.07E+04 27 30 5 1 35 160 9.00E+06 4.27E+05 1.00E+07 5.12E+05 3.12E+06 6.34E+07 6.34E+03 3.02E+04 7.30E+06 7.31E+06 7.32E+06 7.10E+07 1.23E+07 5.14E+03 1.44E+03 3.14E+03 30 5 1.5 20 1.01E+07 7.51E+06 1.640E+07 5.32E+06 1.02E+07	21	30	5	1	20	180	9.077E+06	4.402E+05	1.027E+07	5.077E+05	2.885E+06	-7.385E+06	6.720E-03	6.167E-04
23 30 5 1 35 50 9 216Free 5048Ered 1038Ered 530Ered 3302Ered 7307Ered 6338Ered 633Ered 7307Ered 6338Ered 633Ered 7307Ered 6338Ered 633Ered 730Ered 6338Ered 633Ered 633Ered 932Ered 633Ered 6	22	30	5	1	35	0	9.247E+06	4.245E+05	1.043E+07	4.897E+05	2.853E+06	-7.582E+06	6.505E-03	7.223E-04
24 30 5 1 35 60 1,132E+07 4,293E+05 1,290E+07 4,270E+05 3,295E+06 -8,211E+06 6,313E+03 9,942E+04 25 30 5 1 35 100 1,142E+07 4,271E+05 1,305E+07 5,261E+05 3,393E+06 -8,211E+06 6,313E+03 9,021E+04 27 30 5 1 35 150 9,590E+06 4,721E+05 1,035E+07 5,261E+05 3,392E+06 -7,373E+06 6,446-03 9,021E-04 28 30 5 1.5 20 30 1,240E+07 5,647E+05 1,307E+07 5,216E+06 -1,01E+07 1,01E+02 2,144E-03 2,922E-04 30 5 1.5 20 100 1,240E+07 5,047E+07 5,631E+06 5,249E+06 -1,111E+07 1,232E+02 2,44E+03 31 30 5 1.5 20 100 1,301E+07 5,021E+07 7,34E+05 5,249E+06 -1,102E+07 1,241E+07 1,241E+07	23	30	5	1	35	30	9.216E+06	5.048E+05	1.038E+07	5.628E+05	3.108E+06	-7.597E+06	6.393E-03	1.244E-03
25 30 5 1 35 90 1008E+07 4,743E+05 1.137E+07 5.208E+06 3.821E+06 -8.210E+06 6.344E-03 9.071E+01 26 30 5 1 35 120 1.144E+07 4.971E+05 1.305E+07 5.201E+05 3.821E+06 -9.05E+06 6.444E-03 9.020E+04 28 30 5 1.5 20 0 1.232E+07 6.491E+05 5.741E+06 1.704E-02 3.288E-03 30 5 1.5 20 0 1.237E+07 6.40E+07 7.682H+06 5.774E+06 1.171E+07 1.928E-02 2.14E-02 2.148E-03 31 30 5 1.5 20 0 1.31E+07 7.11E+07 6.83E+05 5.83E+06 -1.171E+07 1.82E+02 2.14E+02 2.14E+03 31 30 5 1.5 20 1.50 1.23E+07 6.37E+07 7.37E+06 1.06E+07 1.73E+02 2.947E+03 34 30 5 1.5 <td>24</td> <td>30</td> <td>5</td> <td>1</td> <td>35</td> <td>60</td> <td>1.132E+07</td> <td>4.293E+05</td> <td>1.290E+07</td> <td>4.570E+05</td> <td>3.932E+06</td> <td>-8.981E+06</td> <td>6.313E-03</td> <td>9.942E-04</td>	24	30	5	1	35	60	1.132E+07	4.293E+05	1.290E+07	4.570E+05	3.932E+06	-8.981E+06	6.313E-03	9.942E-04
26 30 5 1 35 150 9.44E+07 4.971E+05 1.305E+07 5.261E+03 3.122E+06 -9.065E+06 6.23E+03 9.020E+04 27 30 5 1 35 150 9.061E+06 4.27E+05 1.025E+07 4.911E+05 2.880E+06 -7.87E+06 6.123E-03 9.922E+04 30 5 1.5 20 30 1.244E+07 5.647E+05 1.397E+07 6.210E+05 5.249E+06 -1.01E+07 1.74E+02 2.14E+02 2.144E+03 30 5 1.5 20 30 1.200E+07 5.647E+05 1.40E+07 7.31E+05 5.249E+06 -1.01E+07 1.34E+07 31 30 5 1.5 20 100 1.239E+07 6.01E+05 1.447E+07 7.31E+05 6.328E+06 -1.02E+07 1.02E+07 5.04E+05 5.285E+06 -1.02E+07 1.56E+02 2.86E+03 33 0 5 1.5 3 0 1.239E+07 6.07E+05 5.4E+05 <th< td=""><td>25</td><td>30</td><td>5</td><td>1</td><td>35</td><td>90</td><td>1.008E+07</td><td>4.743E+05</td><td>1.137E+07</td><td>5.208E+05</td><td>3.295E+06</td><td>-8.219E+06</td><td>6.394E-03</td><td>9.874E-04</td></th<>	25	30	5	1	35	90	1.008E+07	4.743E+05	1.137E+07	5.208E+05	3.295E+06	-8.219E+06	6.394E-03	9.874E-04
27 30 5 1 35 150 9.590E+06 4.726E+05 1.080E+07 5.169E+05 3.122E+06 -7.878E+06 6.123E-03 9.020E+04 28 30 5 1.5 20 0 1.23E+07 6.21E+07 6.21E+05 5.75E+06 6.102E+03 9.922E+04 30 5 1.5 20 0 1.24E+07 6.540E+05 1.470E+07 5.75E+06 6.406E+06 -9.928E+06 -1.171E+07 1.524E+02 2.144E+03 31 30 5 1.5 20 0 1.310E+07 6.11E+05 1.47E+07 6.532E+05 5.452E+06 -1.171E+07 1.925E+02 2.451E-03 34 30 5 1.5 20 150 1.25E+07 5.46E+07 7.47E+05 5.37E+06 -1.181E+07 1.925E+02 2.461E-03 34 30 5 1.5 35 0 1.232E+07 5.671E+05 1.47E+07 5.27E+06 -1.02E+07 1.71E+02 3.307E+02 1.71E+02 3	26	30	5	1	35	120	1.144E+07	4.971E+05	1.305E+07	5.261E+05	3.982E+06	-9.065E+06	6.544E-03	1.071E-03
28 30 5 1 35 180 9.061E+06 4.27TE+05 1.32E+07 4.911E+05 2.880E+06 -7.373E+06 6.446E+03 9.922E+04 29 30 5 1.5 20 0 1.234E+07 5.647E+05 1.30TE+07 6.210E+05 5.648E+06 -9.928E+06 2.114E+02 2.149E+03 31 30 5 1.5 20 60 1.479E+07 5.160E+05 1.689E+07 5.381E+05 5.249E+06 -1.171E+07 1.825E+02 2.441E-03 32 30 5 1.5 20 150 1.239E+07 6.01E+05 1.37E+07 6.37E+05 6.190E+06 -1.020E+07 1.568E+02 2.842E+03 34 30 5 1.5 30 1.239E+07 5.07E+05 1.47E+07 6.278E+05 5.28E+06 -1.020E+07 1.74E+02 2.947E+03 36 30 5 1.5 35 30 1.247E+07 5.70E+05 5.48E+06 -1.020E+07 1.71E+02 3.307E+02	27	30	5	1	35	150	9.590E+06	4.726E+05	1.080E+07	5.169E+05	3.122E+06	-7.878E+06	6.123E-03	9.020E-04
29 30 5 1.5 20 0 1.234E+07 6.647E+05 1.397E+07 6.210E+05 5.764E+06 -1.001E+07 1.704E+02 2.149E+03 30 30 5 1.5 20 00 1.240E+07 6.580E+05 1.248E+05 5.249E+06 -1.01E+07 1.825E+02 2.249E+06 31 30 5 1.5 20 00 1.301E+07 6.01E+05 1.467E+07 6.73E+05 6.40E+07 1.935E+02 2.243E+03 33 30 5 1.5 20 120 1.494E+07 7.37E+05 1.67E+05 6.10E+07 1.57E+02 2.842E+03 36 30 5 1.5 35 0 1.239E+07 5.071E+05 1.417E+07 6.29E+05 5.27E+06 -1.029E+07 1.734E+02 2.997E+03 37 30 5 1.5 35 0 1.23E+07 5.77E+05 1.447E+07 6.298E+05 5.21E+06 -1.173E+07 1.73E+02 2.996E+03 38	28	30	5	1	35	180	9.061E+06	4.277E+05	1.025E+07	4.911E+05	2.880E+06	-7.373E+06	6.446E-03	9.922E-04
30 5 1.5 20 30 1.240E+07 6.540E+05 1.410E+07 7.162E+05 6.406E+06 -9.928E+06 2.114E-02 2.148E-03 31 30 5 1.5 20 90 1.301E+07 6.540E+05 5.249E+06 -1.171E+07 1.825E+02 2.343E-03 32 30 5 1.5 20 120 1.494E+07 7.053E+05 1.762E+07 5.785E+06 -1.181E+07 1.929E+02 2.461E-03 34 30 5 1.5 20 150 1.239E+07 5.746E+05 1.47E+07 6.376E+05 5.100E+06 -1.020E+07 1.734E-02 2.947E-03 36 30 5 1.5 35 0 1.239E+07 5.746E+05 1.404E+07 6.249E+05 5.854E+06 -1.020E+07 1.734E+02 2.996E-03 38 30 5 1.5 35 0 1.243E+07 5.73E+05 5.261E+06 -1.173E+07 1.853E-02 2.946E-03 38 30 5 <td>29</td> <td>30</td> <td>5</td> <td>1.5</td> <td>20</td> <td>0</td> <td>1.234E+07</td> <td>5.647E+05</td> <td>1.397E+07</td> <td>6.210E+05</td> <td>5.764E+06</td> <td>-1.001E+07</td> <td>1.704E-02</td> <td>3.298E-03</td>	29	30	5	1.5	20	0	1.234E+07	5.647E+05	1.397E+07	6.210E+05	5.764E+06	-1.001E+07	1.704E-02	3.298E-03
31 30 5 1.5 20 60 1.479E+07 5.160E+05 1.689E+07 5.683E+05 5.249E+06 -1.171E+07 1.825E+02 3.144E-03 32 30 5 1.5 20 90 1.301E+07 6.01E+05 1.467E+07 6.731E+05 5.249E+06 -1.164E+07 1.929E-02 2.441E-03 33 30 5 1.5 20 150 1.529E+07 5.746E+05 1.477E+07 6.376E+05 6.100E+07 1.734E-02 2.947E-03 36 30 5 1.5 35 0 1.239E+07 6.571E+05 1.447E+07 6.298E+05 5.527E+06 -1.029E+07 1.734E-02 2.947E-03 37 30 5 1.5 35 0 1.239E+07 6.70E+05 1.447E+07 6.20E+07 5.854E+06 -1.029E+07 1.585E+02 2.996E-03 38 30 5 1.5 35 10 1.247E+07 6.70E+05 7.73E+06 -1.108E+07 1.90E+02 2.242E+03 <td>30</td> <td>30</td> <td>5</td> <td>1.5</td> <td>20</td> <td>30</td> <td>1.240E+07</td> <td>6.540E+05</td> <td>1.410E+07</td> <td>7.162E+05</td> <td>6.406E+06</td> <td>-9.928E+06</td> <td>2.114E-02</td> <td>2.149E-03</td>	30	30	5	1.5	20	30	1.240E+07	6.540E+05	1.410E+07	7.162E+05	6.406E+06	-9.928E+06	2.114E-02	2.149E-03
3 5 1.5 20 90 1.301E+07 6.011E+05 1.467E+07 6.731E+05 7.632E+06 -1.064E+07 1.915E+02 2.543E-03 33 30 5 1.5 20 120 1.494E+07 7.053E+05 1.304E+07 6.731E+05 5.252E+06 -1.064E+07 1.915E+02 2.543E-03 34 30 5 1.5 20 180 1.239E+07 7.053E+05 1.257E+06 -1.020E+07 1.568E-02 2.662E-03 36 5 1.5 35 0 1.239E+07 5.671E+05 1.40E+07 6.238E+05 5.527E+06 -1.032E+07 1.712E-02 3.307E-03 37 30 5 1.5 35 00 1.239E+07 5.671E+05 1.40E+07 5.257E+06 -1.035E+07 1.712E+02 2.307E-03 38 30 5 1.5 35 00 1.30E+07 5.717E+07 5.694E+05 5.297E+06 -1.08E+07 1.961E-02 2.526E-03 40 30 <th< td=""><td>31</td><td>30</td><td>5</td><td>15</td><td>20</td><td>60</td><td>1 479E+07</td><td>5 160E+05</td><td>1 689E+07</td><td>5 683E+05</td><td>5 249E+06</td><td>-1 171E+07</td><td>1 825E-02</td><td>3 144E-03</td></th<>	31	30	5	15	20	60	1 479E+07	5 160E+05	1 689E+07	5 683E+05	5 249E+06	-1 171E+07	1 825E-02	3 144E-03
32 30 5 1.5 20 1.50110 0.01100 </td <td>32</td> <td>30</td> <td>5</td> <td>1.5</td> <td>20</td> <td>90</td> <td>1.301E+07</td> <td>6.011E+05</td> <td>1.467E+07</td> <td>6 731E+05</td> <td>7.632E+06</td> <td>-1.064E+07</td> <td>1.015E-02</td> <td>2 543E-03</td>	32	30	5	1.5	20	90	1.301E+07	6.011E+05	1.467E+07	6 731E+05	7.632E+06	-1.064E+07	1.015E-02	2 543E-03
33 30 3 1.3 20 1.3 1.20 1.491107 1.001107 1.301107 1.201107	22	20	5	1.5	20	120	1.301E+07	7.053E±05	1.407E+07	7.854E+05	5.285E+06	-1.004E+07	1.020E.02	2.545E-05
34 30 35 1.3 20 1.30 1.256F407 6.30EF03 1.39EF07 6.370EF03 6.190EF00 -1.02EF07 1.73EF02 2.482E43 36 30 5 1.5 35 00 1.256F407 5.746E+05 1.417E+07 6.249E+05 5.854E+06 -1.02E+07 1.71E+02 3.307E+03 37 30 5 1.5 35 00 1.236E+07 5.71E+05 1.417E+07 7.202E+05 6.614E+06 -9.975E+06 2.187E+02 1.996E+03 38 30 5 1.5 35 00 1.366E+07 5.173E+05 1.692E+07 5.694E+05 5.207E+06 -1.173E+07 1.853E+02 2.296E+03 40 30 5 1.5 35 120 1.497E+07 6.976E+05 1.472E+07 6.347E+06 -1.022E+07 1.698E+07 2.818E+03 41 30 15 0.5 20 0 2.107E+07 9.481E+05 2.142E+07 1.008E+06 6.697E+06 -1.22E+07	24	20	5	1.5	20	120	1.494E+07	7.055E+05	1.700E+07	6.276E+05	5.285E+00	-1.181E+07	1.929E-02	2.401E-03
35 30 5 1.5 20 180 1.239E+07 5.671E+05 1.417E+07 6.249E+05 5.824E+06 -1.095E+06 2.18E+02 1.39E+02 2.997E+03 37 30 5 1.5 35 00 1.239E+07 5.671E+05 1.40E+07 6.249E+05 5.854E+06 -1.095E+06 2.187E+02 1.996E+03 38 30 5 1.5 35 60 1.432E+07 5.173E+05 1.692E+07 5.694E+05 5.261E+06 -1.173E+07 1.853E+02 2.996E+03 40 30 5 1.5 35 90 1.205E+07 6.06E+05 1.705E+05 5.297E+06 -1.184E+07 2.000E+02 2.221E+03 41 30 5 1.5 35 180 1.259E+07 5.764E+05 1.398E+07 6.416E+05 6.347E+06 -1.032E+07 1.558E+02 2.847E+03 42 30 15 0.5 20 0 2.001E+07 9.048E+05 2.377E+07 1.003E+06 7.757E+06 -1.720E+07 1.408E+02 1.782E+03 43 30 15	34 25	30	5	1.5	20	100	1.239E+07	6.031E+03	1.394E+07	6.3/0E+05	6.190E+06	-1.020E+07	1.308E-02	2.862E-03
36 30 5 1.5 35 0 1.239E+07 5.671E+05 1.404E+07 6.239E+05 5.834E+06 -1.005E+07 1.712E+02 3.307E+03 37 30 5 1.5 35 30 1.247E+07 6.570E+05 1.417E+07 7.202E+05 6.614E+06 -9.975E+06 2.187E+02 2.996E+03 39 30 5 1.5 35 90 1.306E+07 6.173E+05 1.692E+07 5.694E+05 5.20E1E+06 -1.18E+07 2.00E+02 2.296E-03 40 30 5 1.5 35 120 1.497E+07 6.976E+05 1.709E+07 7.512E+05 5.297E+06 -1.18E+07 2.006E+02 2.287E+03 41 30 5 1.5 35 180 1.259E+07 5.64E+05 1.421E+07 6.31E+05 5.61E+06 -1.032E+07 1.73E+02 2.81E+03 43 30 15 0.5 20 30 1.896E+07 9.481E+05 2.142E+07 1.098E+06 6.697E+06	35	30	5	1.5	20	180	1.256E+07	5./46E+05	1.41/E+0/	6.298E+05	5.52/E+06	-1.029E+07	1./34E-02	2.94/E-03
37 30 5 1.5 35 30 1.247E+07 6.570E+05 1.417E+07 7.202E+05 6.614E+06 -9.975E+06 2.187E-02 1.996E-03 38 30 5 1.5 35 60 1.482E+07 5.173E+05 1.692E+07 5.694E+05 5.261E+06 -1.173E+07 1.853E-02 2.996E-03 40 30 5 1.5 35 10 1.243E+07 6.956E+05 1.709E+07 7.512E+05 5.297E+06 -1.184E+07 2.000E-02 2.291E-03 41 30 5 1.5 35 180 1.2359E+07 5.764E+05 1.398E+07 6.416E+05 6.347E+06 -1.032E+07 1.753E+02 2.817E+03 43 30 15 0.5 20 0 2.107E+07 9.048E+05 2.377E+07 1.003E+06 6.697E+06 -1.550E+07 1.408E+02 1.782E-03 44 30 15 0.5 20 60 2.001E+07 6.491E+05 2.337E+07 9.639E+05 7.30E+06 <td>36</td> <td>30</td> <td>5</td> <td>1.5</td> <td>35</td> <td>0</td> <td>1.239E+07</td> <td>5.671E+05</td> <td>1.404E+07</td> <td>6.249E+05</td> <td>5.854E+06</td> <td>-1.005E+07</td> <td>1.712E-02</td> <td>3.307E-03</td>	36	30	5	1.5	35	0	1.239E+07	5.671E+05	1.404E+07	6.249E+05	5.854E+06	-1.005E+07	1.712E-02	3.307E-03
38 30 5 1.5 35 60 1.432E+07 5.173E+05 1.692E+07 5.694E+05 5.261E+06 -1.173E+07 1.833E-02 2.996E-03 39 30 5 1.5 35 90 1.306E+07 6.036E+05 1.472E+07 6.760E+05 7.735E+06 -1.068E+07 1.991E-02 2.526E-03 40 30 5 1.5 35 120 1.497E+07 6.976E+05 1.798E+07 6.416E+05 6.347E+06 -1.032E+07 1.555E-02 2.847E-03 42 30 5 1.5 35 180 1.259E+07 5.764E+05 1.421E+07 6.331E+05 5.616E+06 -1.032E+07 1.758E-02 2.847E-03 44 30 15 0.5 20 30 1.896E+07 9.481E+05 2.377E+07 1.003E+06 7.57E+06 -1.50E+07 1.389E-02 2.147E-03 45 30 15 0.5 20 100 1.981E+07 8.438E+05 2.237E+07 9.663E+05 7.262E+06 <td>37</td> <td>30</td> <td>5</td> <td>1.5</td> <td>35</td> <td>30</td> <td>1.247E+07</td> <td>6.570E+05</td> <td>1.417E+07</td> <td>7.202E+05</td> <td>6.614E+06</td> <td>-9.975E+06</td> <td>2.187E-02</td> <td>1.996E-03</td>	37	30	5	1.5	35	30	1.247E+07	6.570E+05	1.417E+07	7.202E+05	6.614E+06	-9.975E+06	2.187E-02	1.996E-03
39 30 5 1.5 35 90 1.306E+07 6.036E+05 1.472E+07 6.760E+05 7.735E+06 -1.068E+07 1.961E-02 2.526E-03 40 30 5 1.5 35 120 1.497E+07 6.056E+05 1.709E+07 7.512E+05 5.297E+06 -1.184E+07 2.000E-02 2.291E-03 41 30 5 1.5 35 150 1.243E+07 6.054E+05 1.398E+07 6.416E+05 6.347E+06 -1.032E+07 1.555E-02 2.813E-03 43 30 15 0.5 20 0 2.107E+07 9.048E+05 2.377E+07 1.003E+06 7.57E+06 -1.720E+07 1.389E-02 2.147E+03 44 30 15 0.5 20 60 2.001E+07 6.141E+05 2.237E+07 1.003E+06 7.57E+06 -1.617E+07 1.389E-02 2.147E+03 46 30 15 0.5 20 19.01E+07 8.458E+05 2.237E+07 7.00E+06 7.1617E+07 1.338E	38	30	5	1.5	35	60	1.482E+07	5.173E+05	1.692E+07	5.694E+05	5.261E+06	-1.173E+07	1.853E-02	2.996E-03
40 30 5 1.5 35 120 1.497E+07 6.976E+05 1.709E+07 7.512E+05 5.297E+06 -1.184E+07 2.000E-02 2.291E-03 41 30 5 1.5 35 150 1.243E+07 6.054E+05 1.398E+07 6.416E+05 6.347E+06 -1.023E+07 1.753E+02 2.847E+03 42 30 15 0.5 20 0 2.107E+07 5.764E+05 1.421E+07 6.031E+05 5.616E+06 -1.032E+07 1.753E+02 2.813E+03 43 30 15 0.5 20 30 1.896E+07 9.841E+05 2.142E+07 1.098E+06 6.697E+06 -1.550E+07 1.360E-02 1.623E+03 44 30 15 0.5 20 60 2.001E+07 6.141E+05 2.237E+07 9.639E+05 7.00E+06 -1.617E+07 1.360E-02 2.304E+03 47 30 15 0.5 20 150 1.963E+07 8.339E+05 2.200E+07 9.062E+05 6.732E+06 -1.629E+07 1.617E+02 1.393E+03 1.392E+03 1.392E+03 1.393E+03 </td <td>39</td> <td>30</td> <td>5</td> <td>1.5</td> <td>35</td> <td>90</td> <td>1.306E+07</td> <td>6.036E+05</td> <td>1.472E+07</td> <td>6.760E+05</td> <td>7.735E+06</td> <td>-1.068E+07</td> <td>1.961E-02</td> <td>2.526E-03</td>	39	30	5	1.5	35	90	1.306E+07	6.036E+05	1.472E+07	6.760E+05	7.735E+06	-1.068E+07	1.961E-02	2.526E-03
41 30 5 1.5 35 150 1.243E+07 6.054E+05 1.398E+07 6.416E+05 6.347E+06 -1.023E+07 1.555E-02 2.847E-03 42 30 15 0.5 20 0 2.107E+07 9.048E+05 2.377E+07 1.003E+06 7.757E+06 -1.720E+07 1.408E+02 1.782E+03 44 30 15 0.5 20 0 2.107E+07 9.048E+05 2.377E+07 1.003E+06 7.757E+06 -1.720E+07 1.408E+02 2.147E+03 45 30 15 0.5 20 60 2.001E+07 6.141E+05 2.237E+07 6.691E+05 7.341E+06 -1.645E+07 1.368E+02 2.304E+03 46 30 15 0.5 20 190 1.981E+07 8.458E+05 2.237E+07 9.639E+05 7.00E+06 -1.617E+07 1.368E+02 2.304E+03 48 30 15 0.5 20 150 1.963E+07 8.392E+05 2.308E+07 9.052E+05 6.732E+06 -1.629E+07 1.617E-02 1.939E+03 49 30 15 <td>40</td> <td>30</td> <td>5</td> <td>1.5</td> <td>35</td> <td>120</td> <td>1.497E+07</td> <td>6.976E+05</td> <td>1.709E+07</td> <td>7.512E+05</td> <td>5.297E+06</td> <td>-1.184E+07</td> <td>2.000E-02</td> <td>2.291E-03</td>	40	30	5	1.5	35	120	1.497E+07	6.976E+05	1.709E+07	7.512E+05	5.297E+06	-1.184E+07	2.000E-02	2.291E-03
42 30 5 1.5 35 180 1.259E+07 5.764E+05 1.421E+07 6.331E+05 5.616E+06 -1.032E+07 1.753E+02 2.813E-03 43 30 15 0.5 20 0 2.107E+07 9.048E+05 2.377E+07 1.003E+06 7.757E+06 -1.720E+07 1.408E+02 1.782E+03 44 30 15 0.5 20 30 1.896E+07 9.841E+05 2.142E+07 1.098E+06 6.697E+06 -1.550E+07 1.389E-02 2.147E+03 45 30 15 0.5 20 60 2.001E+07 6.141E+05 2.237E+07 9.639E+05 7.000E+06 -1.645E+07 1.538E+02 2.304E+03 47 30 15 0.5 20 120 1.900E+07 6.059E+05 2.142E+07 9.652E+05 7.262E+06 -1.629E+07 1.617E-02 1.939E+03 48 30 15 0.5 20 180 2.115E+07 8.832E+05 2.308E+07 9.062E+05 6.732E+06 -1.727E+07 1.338E+02 2.112E+03 50 30 15 </td <td>41</td> <td>30</td> <td>5</td> <td>1.5</td> <td>35</td> <td>150</td> <td>1.243E+07</td> <td>6.054E+05</td> <td>1.398E+07</td> <td>6.416E+05</td> <td>6.347E+06</td> <td>-1.023E+07</td> <td>1.555E-02</td> <td>2.847E-03</td>	41	30	5	1.5	35	150	1.243E+07	6.054E+05	1.398E+07	6.416E+05	6.347E+06	-1.023E+07	1.555E-02	2.847E-03
43 30 15 0.5 20 0 2.107E+07 9.048E+05 2.377E+07 1.003E+06 7.757E+06 -1.720E+07 1.408E+02 1.782E-03 44 30 15 0.5 20 30 1.896E+07 9.841E+05 2.142E+07 1.098E+06 6.697E+06 -1.550E+07 1.389E-02 2.147E-03 45 30 15 0.5 20 60 2.001E+07 6.141E+05 2.253E+07 6.691E+05 7.341E+06 -1.645E+07 1.580E-02 2.304E-03 46 30 15 0.5 20 90 1.981E+07 8.458E+05 2.237E+07 9.639E+05 7.000E+06 -1.617E+07 1.538E-02 2.304E-03 47 30 15 0.5 20 120 1.900E+07 6.059E+05 2.142E+07 6.585E+05 7.262E+06 -1.629E+07 1.617E+02 1.939E-03 49 30 15 0.5 20 180 2.115E+07 8.33E+05 2.385E+07 1.098E+06 9.086E+06 -1.727E+07 1.33E-02 2.121E+03 50 30 15 <td>42</td> <td>30</td> <td>5</td> <td>1.5</td> <td>35</td> <td>180</td> <td>1.259E+07</td> <td>5.764E+05</td> <td>1.421E+07</td> <td>6.331E+05</td> <td>5.616E+06</td> <td>-1.032E+07</td> <td>1.753E-02</td> <td>2.813E-03</td>	42	30	5	1.5	35	180	1.259E+07	5.764E+05	1.421E+07	6.331E+05	5.616E+06	-1.032E+07	1.753E-02	2.813E-03
44 30 15 0.5 20 30 1.896E+07 9.841E+05 2.142E+07 1.098E+06 6.697E+06 -1.550E+07 1.389E-02 2.147E-03 45 30 15 0.5 20 60 2.001E+07 6.141E+05 2.253E+07 6.691E+05 7.341E+06 -1.645E+07 1.360E-02 1.623E-03 46 30 15 0.5 20 120 1.900E+07 6.059E+05 2.142E+07 6.585E+05 7.262E+06 -1.617E+07 1.538E-02 2.211E-03 48 30 15 0.5 20 150 1.963E+07 8.339E+05 2.200E+07 9.062E+05 6.732E+06 -1.629E+07 1.617E+02 1.939E-03 49 30 15 0.5 35 0 2.115E+07 8.803E+05 2.385E+07 1.089E+06 9.086E+06 -1.725E+07 1.338E-02 2.112E-03 50 30 15 0.5 35 0 2.177E+07 1.076E+06 2.465E+07 1.193E+06 7.468E+06 -1.757E+07 1.336E-02 2.070E+03 51 30 15 <td>43</td> <td>30</td> <td>15</td> <td>0.5</td> <td>20</td> <td>0</td> <td>2.107E+07</td> <td>9.048E+05</td> <td>2.377E+07</td> <td>1.003E+06</td> <td>7.757E+06</td> <td>-1.720E+07</td> <td>1.408E-02</td> <td>1.782E-03</td>	43	30	15	0.5	20	0	2.107E+07	9.048E+05	2.377E+07	1.003E+06	7.757E+06	-1.720E+07	1.408E-02	1.782E-03
45 30 15 0.5 20 60 2.001E+07 6.141E+05 2.233E+07 6.691E+05 7.341E+06 -1.645E+07 1.360E-02 2.304E-03 46 30 15 0.5 20 90 1.981E+07 8.458E+05 2.237E+07 9.639E+05 7.000E+06 -1.617E+07 1.538E-02 2.304E-03 47 30 15 0.5 20 120 1.900E+07 6.059E+05 2.142E+07 6.585E+05 7.262E+06 -1.629E+07 1.617E+02 1.939E-03 48 30 15 0.5 20 180 2.115E+07 8.803E+05 2.385E+07 9.062E+05 6.732E+06 -1.629E+07 1.617E+02 1.939E-03 50 30 15 0.5 35 0 2.115E+07 9.818E+05 2.385E+07 1.089E+06 9.086E+06 -1.727E+07 1.338E+02 2.070E+03 51 30 15 0.5 35 30 2.177E+07 1.076E+06 2.465E+07 1.193E+06 7.468E+06 -1.615E+07 1.349E+02 1.452E+03 53 30 15 </td <td>44</td> <td>30</td> <td>15</td> <td>0.5</td> <td>20</td> <td>30</td> <td>1.896E+07</td> <td>9.841E+05</td> <td>2.142E+07</td> <td>1.098E+06</td> <td>6.697E+06</td> <td>-1.550E+07</td> <td>1.389E-02</td> <td>2.147E-03</td>	44	30	15	0.5	20	30	1.896E+07	9.841E+05	2.142E+07	1.098E+06	6.697E+06	-1.550E+07	1.389E-02	2.147E-03
46 30 15 0.5 20 90 1.981E+07 8.458E+05 2.237E+07 9.639E+05 7.000E+06 -1.617E+07 1.538E-02 2.304E-03 47 30 15 0.5 20 120 1.900E+07 6.059E+05 2.142E+07 6.585E+05 7.262E+06 -1.565E+07 1.269E-02 2.211E-03 48 30 15 0.5 20 150 1.963E+07 8.339E+05 2.200E+07 9.062E+05 6.732E+06 -1.629E+07 1.617E-02 1.939E-03 49 30 15 0.5 20 180 2.115E+07 8.803E+05 2.385E+07 9.076E+05 7.935E+06 -1.727E+07 1.358E-02 2.112E-03 50 30 15 0.5 35 0 2.117E+07 1.076E+06 2.465E+07 1.193E+06 7.468E+06 -1.757E+07 1.336E-02 2.070E-03 51 30 15 0.5 35 60 2.009E+07 6.163E+05 2.261E+07 6.718E+05 7.19E+06 -1.616E+07 1.501E-02 1.994E-03 53 30 15 </td <td>45</td> <td>30</td> <td>15</td> <td>0.5</td> <td>20</td> <td>60</td> <td>2.001E+07</td> <td>6.141E+05</td> <td>2.253E+07</td> <td>6.691E+05</td> <td>7.341E+06</td> <td>-1.645E+07</td> <td>1.360E-02</td> <td>1.623E-03</td>	45	30	15	0.5	20	60	2.001E+07	6.141E+05	2.253E+07	6.691E+05	7.341E+06	-1.645E+07	1.360E-02	1.623E-03
4730150.5201201.900E+076.059E+052.142E+076.585E+057.262E+06-1.565E+071.269E-022.211E-034830150.5201501.963E+078.339E+052.200E+079.062E+056.732E+06-1.629E+071.617E-021.939E-034930150.5201802.115E+078.803E+052.385E+079.776E+057.935E+06-1.725E+071.358E-022.112E-035030150.53502.115E+079.818E+052.385E+071.089E+069.086E+06-1.727E+071.338E-022.070E-035130150.53502.177E+071.076E+062.465E+071.193E+067.468E+06-1.651E+071.336E-022.070E-035230150.535602.009E+076.163E+052.237E+071.045E+068.186E+06-1.616E+071.501E-021.994E+035330150.5351201.999E+076.081E+052.152E+076.607E+057.804E+06-1.616E+071.306E-022.101E-035430150.5351501.964E+078.337E+052.200E+079.059E+057.122E+06-1.631E+071.638E-021.772E-035530150.5351802.122E+079.591E+052.393E+071.077E+069.260E+06-1.732E+071.638E-022.041E-035630150.5<	46	30	15	0.5	20	90	1.981E+07	8.458E+05	2.237E+07	9.639E+05	7.000E+06	-1.617E+07	1.538E-02	2.304E-03
48 30 15 0.5 20 150 1.963E+07 8.339E+05 2.200E+07 9.062E+05 6.732E+06 -1.629E+07 1.617E-02 1.939E-03 49 30 15 0.5 20 180 2.115E+07 8.803E+05 2.385E+07 9.776E+05 7.935E+06 -1.725E+07 1.358E-02 2.112E-03 50 30 15 0.5 35 0 2.115E+07 9.818E+05 2.385E+07 1.089E+06 9.086E+06 -1.727E+07 1.338E-02 2.132E-03 51 30 15 0.5 35 0 2.117E+07 1.076E+06 2.465E+07 1.193E+06 7.468E+06 -1.727E+07 1.336E-02 2.070E-03 52 30 15 0.5 35 60 2.009E+07 6.163E+05 2.261E+07 6.718E+05 7.719E+06 -1.651E+07 1.336E-02 2.070E-03 53 30 15 0.5 35 90 1.981E+07 9.563E+05 2.237E+07 1.045E+06 8.186E+06 -1.616E+07 1.501E-02 1.994E-03 54 30 15 <td>47</td> <td>30</td> <td>15</td> <td>0.5</td> <td>20</td> <td>120</td> <td>1.900E+07</td> <td>6.059E+05</td> <td>2.142E+07</td> <td>6.585E+05</td> <td>7.262E+06</td> <td>-1.565E+07</td> <td>1.269E-02</td> <td>2.211E-03</td>	47	30	15	0.5	20	120	1.900E+07	6.059E+05	2.142E+07	6.585E+05	7.262E+06	-1.565E+07	1.269E-02	2.211E-03
A9 30 15 0.5 20 180 2.150E107 8.803E107 9.706E107 9.776E105 7.935E106 -1.725E107 1.358E02 2.112E-03 50 30 15 0.5 35 0 2.115E107 8.803E105 2.385E107 9.776E105 7.935E106 -1.725E107 1.358E02 2.112E-03 50 30 15 0.5 35 0 2.115E107 9.818E405 2.385E407 1.089E406 9.086E406 -1.727E407 1.338E02 2.1389E-03 51 30 15 0.5 35 60 2.009E407 6.163E405 2.261E407 6.718E405 7.719E406 -1.651E407 1.349E-02 1.452E-03 53 30 15 0.5 35 90 1.981E407 9.563E405 2.237E407 1.045E406 8.186E406 -1.616E407 1.501E02 1.994E-03 54 30 15 0.5 35 120 1.999E407 6.081E407 9.059E407 9.059E405 7.122E406 -1.616E407 1.501E02 2.101E-03 55 30 15	48	30	15	0.5	20	150	1 963E+07	8 339E+05	2 200E+07	9.062E+05	6 732E+06	-1 629E+07	1.617E-02	1 939E-03
50 15 0.5 160 2.112E+07 0.005E+05 2.005E+07 1.089E+06 9.086E+06 -1.125E+07 1.338E+02 1.389E-02 1.389E-02 1.389E-03 50 30 15 0.5 35 0 2.115E+07 9.818E+05 2.385E+07 1.089E+06 9.086E+06 -1.727E+07 1.333E-02 1.389E-03 51 30 15 0.5 35 30 2.177E+07 1.076E+06 2.465E+07 1.193E+06 7.468E+06 -1.757E+07 1.336E-02 2.070E-03 52 30 15 0.5 35 60 2.009E+07 6.163E+05 2.261E+07 6.718E+05 7.719E+06 -1.651E+07 1.349E-02 1.452E-03 53 30 15 0.5 35 90 1.981E+07 9.563E+05 2.237E+07 1.045E+06 8.186E+06 -1.616E+07 1.501E+02 1.994E+03 54 30 15 0.5 35 150 1.964E+07 8.337E+05 2.200E+07 9.059E+05 7.122E+06 -1.631E+07 1.638E+02 1.772E+03 1.243E+02 2.041E+03	49	30	15	0.5	20	180	2 115E+07	8 803E+05	2.200E+07	9.776E+05	7 935E+06	-1 725E+07	1.358E-02	2 112E-03
50 50 15 0.5 35 0 2.112E107 9.618E105 2.35E107 1.032E106 9.036E106 -1.127E107 1.532E-02 1.532E-02 1.532E-02 1.532E-02 2.070E-03 51 30 15 0.5 35 60 2.009E+07 6.163E+05 2.261E+07 6.718E+05 7.719E+06 -1.651E+07 1.336E-02 2.070E-03 53 30 15 0.5 35 60 2.009E+07 6.163E+05 2.261E+07 6.718E+05 7.719E+06 -1.651E+07 1.349E-02 1.452E-03 54 30 15 0.5 35 120 1.99E+07 6.081E+05 2.152E+07 6.607E+05 7.804E+06 -1.616E+07 1.501E-02 1.994E-03 55 30 15 0.5 35 150 1.964E+07 8.337E+05 2.200E+07 9.059E+05 7.122E+06 -1.631E+07 1.638E-02 1.772E-03 56 30 15 0.5 35 180 2.122E+07 9.591E+05 2.393E+07 1.077E+06 9.260E+06 -1.732E+07 1.243E-02 2.041E-03<	50	20	15	0.5	25	0	2.115E+07	0.818E±05	2.305E+07	1.080E+06	0.086E±06	1 727E+07	1.333E-02	1 280E 02
31 30 15 0.5 35 30 2.177E+07 1.076E+06 2.403E+07 1.193E+06 7.468E+06 -1.77FE+07 1.336E+02 2.076E+03 52 30 15 0.5 35 60 2.009E+07 6.163E+05 2.261E+07 6.718E+05 7.719E+06 -1.651E+07 1.349E+02 1.452E+03 53 30 15 0.5 35 90 1.981E+07 9.563E+05 2.237E+07 1.045E+06 8.186E+06 -1.616E+07 1.501E+02 1.994E+03 54 30 15 0.5 35 120 1.909E+07 6.081E+05 2.152E+07 6.607E+05 7.804E+06 -1.616E+07 1.306E+02 2.101E+03 55 30 15 0.5 35 150 1.964E+07 8.337E+05 2.200E+07 9.059E+05 7.122E+06 -1.631E+07 1.638E+02 1.772E+03 56 30 15 0.5 35 180 2.122E+07 9.591E+05 2.393E+07 1.077E+06 9.260E+06 -1.732E+07 1.243E+02 2.041E+03 57 30 15	51	20	15	0.5	25	20	2.113E+07	9.818E+05	2.385E+07	1.089E+06	7.468E+06	-1.727E+07	1.335E-02	1.389E-03
52 30 15 0.5 35 60 2.009E+07 6.163E+05 2.261E+07 6.718E+05 7.719E+06 -1.651E+07 1.349E+02 1.452E+03 53 30 15 0.5 35 90 1.981E+07 9.563E+05 2.237E+07 1.045E+06 8.186E+06 -1.616E+07 1.501E+02 1.994E+03 54 30 15 0.5 35 120 1.909E+07 6.081E+05 2.152E+07 6.607E+05 7.804E+06 -1.570E+07 1.306E+02 2.101E+03 55 30 15 0.5 35 150 1.964E+07 8.337E+05 2.200E+07 9.059E+05 7.122E+06 -1.631E+07 1.638E+02 1.772E+03 56 30 15 0.5 35 180 2.122E+07 9.591E+05 2.393E+07 1.077E+06 9.260E+06 -1.732E+07 1.243E+02 2.041E+03 57 30 15 1 20 0 7.361E+06 1.625E+06 7.910E+06 1.876E+06 1.155E+06 -7.454E+06 6.249E+03 1.231E+03 58 30 15 <td>51</td> <td>30</td> <td>15</td> <td>0.5</td> <td>35</td> <td>50</td> <td>2.1//E+0/</td> <td>1.070E+00</td> <td>2.403E+07</td> <td>1.193E+00</td> <td>7.408E+00</td> <td>-1./3/E+0/</td> <td>1.330E-02</td> <td>2.070E-03</td>	51	30	15	0.5	35	50	2.1//E+0/	1.070E+00	2.403E+07	1.193E+00	7.408E+00	-1./3/E+0/	1.330E-02	2.070E-03
53 30 15 0.5 35 90 1.981E+07 9.563E+05 2.237E+07 1.045E+06 8.186E+06 -1.616E+07 1.501E-02 1.994E-03 54 30 15 0.5 35 120 1.909E+07 6.081E+05 2.152E+07 6.607E+05 7.804E+06 -1.570E+07 1.306E-02 2.101E-03 55 30 15 0.5 35 150 1.964E+07 8.337E+05 2.200E+07 9.059E+05 7.122E+06 -1.631E+07 1.638E-02 1.772E-03 56 30 15 0.5 35 180 2.122E+07 9.591E+05 2.393E+07 1.077E+06 9.260E+06 -1.732E+07 1.243E-02 2.041E-03 57 30 15 1 20 0 7.361E+06 1.625E+06 7.910E+06 1.876E+06 1.155E+06 -7.454E+06 6.249E-03 1.231E-03 58 30 15 1 20 30 7.331E+06 1.792E+06 7.884E+06 2.020E+06 1.204E+06 -7.414E+06 6.195E-03 1.239E-03 59 30 15	52	30	15	0.5	35	60	2.009E+07	0.163E+05	2.201E+07	0./18E+05	7.719E+06	-1.051E+07	1.549E-02	1.452E-03
54 30 15 0.5 35 120 1.909E+07 6.081E+05 2.152E+07 6.607E+05 7.804E+06 -1.570E+07 1.306E-02 2.101E-03 55 30 15 0.5 35 150 1.964E+07 8.337E+05 2.200E+07 9.059E+05 7.122E+06 -1.631E+07 1.638E-02 1.772E-03 56 30 15 0.5 35 180 2.122E+07 9.591E+05 2.393E+07 1.077E+06 9.260E+06 -1.732E+07 1.243E-02 2.041E-03 57 30 15 1 20 0 7.361E+06 1.625E+06 7.910E+06 1.876E+06 1.155E+06 -7.454E+06 6.249E-03 1.231E-03 58 30 15 1 20 30 7.331E+06 1.792E+06 7.884E+06 2.020E+06 1.204E+06 -7.414E+06 6.195E-03 1.239E-03 59 30 15 1 20 60 7.499E+06 1.590E+06 8.204E+06 1.836E+06 1.198E+06 -7.695E+06 6.138E-03 1.239E-03 60 30 15	53	30	15	0.5	35	90	1.981E+07	9.563E+05	2.237E+07	1.045E+06	8.186E+06	-1.616E+07	1.501E-02	1.994E-03
55 30 15 0.5 35 150 1.964E+07 8.337E+05 2.200E+07 9.059E+05 7.122E+06 -1.631E+07 1.638E-02 1.772E-03 56 30 15 0.5 35 180 2.122E+07 9.591E+05 2.393E+07 1.077E+06 9.260E+06 -1.732E+07 1.243E-02 2.041E-03 57 30 15 1 20 0 7.361E+06 1.625E+06 7.910E+06 1.876E+06 1.155E+06 -7.454E+06 6.249E-03 1.231E-03 58 30 15 1 20 30 7.331E+06 1.792E+06 7.884E+06 2.020E+06 1.204E+06 -7.414E+06 6.195E-03 1.239E-03 59 30 15 1 20 60 7.499E+06 1.590E+06 8.204E+06 1.836E+06 1.198E+06 -7.695E+06 6.138E-03 1.250E-03 60 30 15 1 20 90 7.419E+06 1.608E+06 7.967E+06 1.840E+06 1.224E+06 -7.516E+06 6.204E-03 1.213E-03	54	30	15	0.5	35	120	1.909E+07	6.081E+05	2.152E+07	6.607E+05	7.804E+06	-1.570E+07	1.306E-02	2.101E-03
56 30 15 0.5 35 180 2.122E+07 9.591E+05 2.393E+07 1.077E+06 9.260E+06 -1.732E+07 1.243E-02 2.041E-03 57 30 15 1 20 0 7.361E+06 1.625E+06 7.910E+06 1.876E+06 1.155E+06 -7.454E+06 6.249E-03 1.231E-03 58 30 15 1 20 30 7.331E+06 1.792E+06 7.884E+06 2.020E+06 1.204E+06 -7.414E+06 6.195E-03 1.239E-03 59 30 15 1 20 60 7.499E+06 1.590E+06 8.204E+06 1.836E+06 1.198E+06 -7.695E+06 6.138E-03 1.250E-03 60 30 15 1 20 90 7.419E+06 1.608E+06 1.840E+06 1.224E+06 -7.516E+06 6.204E-03 1.213E-03	55	30	15	0.5	35	150	1.964E+07	8.337E+05	2.200E+07	9.059E+05	7.122E+06	-1.631E+07	1.638E-02	1.772E-03
57 30 15 1 20 0 7.361E+06 1.625E+06 7.910E+06 1.876E+06 1.155E+06 -7.454E+06 6.249E+03 1.231E+03 58 30 15 1 20 30 7.331E+06 1.792E+06 7.884E+06 2.020E+06 1.204E+06 -7.414E+06 6.195E+03 1.239E+03 59 30 15 1 20 60 7.499E+06 1.590E+06 8.204E+06 1.836E+06 1.198E+06 -7.695E+06 6.138E+03 1.250E+03 60 30 15 1 20 90 7.419E+06 1.608E+06 7.967E+06 1.840E+06 1.224E+06 -7.516E+06 6.204E+03 1.213E+03	56	30	15	0.5	35	180	2.122E+07	9.591E+05	2.393E+07	1.077E+06	9.260E+06	-1.732E+07	1.243E-02	2.041E-03
58 30 15 1 20 30 7.331E+06 1.792E+06 7.884E+06 2.020E+06 1.204E+06 -7.414E+06 6.195E-03 1.239E-03 59 30 15 1 20 60 7.499E+06 1.590E+06 8.204E+06 1.836E+06 1.198E+06 -7.695E+06 6.138E-03 1.250E-03 60 30 15 1 20 90 7.419E+06 1.608E+06 7.967E+06 1.840E+06 1.224E+06 -7.516E+06 6.204E-03 1.213E-03	57	30	15	1	20	0	7.361E+06	1.625E+06	7.910E+06	1.876E+06	1.155E+06	-7.454E+06	6.249E-03	1.231E-03
59 30 15 1 20 60 7.499E+06 1.590E+06 8.204E+06 1.836E+06 1.198E+06 -7.695E+06 6.138E-03 1.250E-03 60 30 15 1 20 90 7.419E+06 1.608E+06 7.967E+06 1.840E+06 1.224E+06 -7.516E+06 6.204E-03 1.213E-03	58	30	15	1	20	30	7.331E+06	1.792E+06	7.884E+06	2.020E+06	1.204E+06	-7.414E+06	6.195E-03	1.239E-03
60 30 15 1 20 90 7.419E+06 1.608E+06 7.967E+06 1.840E+06 1.224E+06 -7.516E+06 6.204E-03 1.213E-03	59	30	15	1	20	60	7.499E+06	1.590E+06	8.204E+06	1.836E+06	1.198E+06	-7.695E+06	6.138E-03	1.250E-03
	60	30	15	1	20	90	7.419E+06	1.608E+06	7.967E+06	1.840E+06	1.224E+06	-7.516E+06	6.204E-03	1.213E-03

(Units - 1: cm, 2: m, 3: GPa, 4: °, 5-10: N/m2, 11-12:m)

 Table 4 Determination of neurons for hidden layers of neural networks

Reference	Equation	This Study
Hush, 1989[55]	3*N.I.N ¹	15
Hecht-Nielsen, 1987[56]	\geq 2*N.I.N+1	≥ 11
Kanellopoulas and Wilkinson, 1997 [57]	2*N.I.N	10
Wang C, 1994[58]	2*N.I.N/3	≈3
Masters, 1994 [59]	(N.I.N*N.O.N ²)^0.5	≈2

1: N.I.N: Number of Input Neurons; 2: N.O.N: Number of Output Neurons

Thereafter, these neurons must be arranged in one or two hidden layer. Theoretically, only one hidden layer is enough for networks with Back Propagation (BP) algorithms [45, 56], but to solve some problems a neural network with two hidden layers is required [45, 59]. In some cases, application of neural networks with more than two hidden layers is useful [57] . Flood and Kartan [49] stated that MLP model with at least two hidden layers provides more flexibility for modelling complex problems. So, different arrangement of 11 neurons were considered in two hidden layers. Based on two transform functions (TANSIG and LOGSIG) resulted RMSE values are summarized in Table 5. It can be seen that model has the best performance in 5-7-4-1 neuron arrangement based on minimum RMSE value.



Fig. 8 Optimum number of neurons in hidden layer(s) based on minimum value for RMSE

Fable 5 Optimum arrangement	of neurons	in two	hidden layers
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No.	NY . N .	RMSE Error					
	Network Arrange- ment	Transfer Function: TANSIG	Transfer Function: LOGSIG				
1	5-[3-8]-1	0.123	0.119				
2	5-[4-7]-1	0.082	0.098				
3	5-[5-6]-1	0.075	0.088				
4	5-[6-5]-1	0.053	0.060				
5	5-[7-4]-1	0.041	0.055				
6	5-[8-3]-1	0.074	0.085				



Fig. 9 Optimized structure of the artificial neural network

7 Sensitivity Analysis

Sensitivity analysis was performed to identify the influence of each input variable on output parameters. A useful method is the CAM (cosine amplitude method) [60, 61]. Data samples form a data vector, X, defined as:

$$X = \{x_1, x_2, x_3, \dots, x_n\}$$

Each of the components x_i in the data vector X, is a vector with length m, i.e.,

$$x_i = \{x_{i1}, x_{i2}, x_{i3}, \dots, x_{im}\}$$

Hence, each data can be assumed as a point in m-dimensional space, where each point needs m coordinates for a full description. Each element of a relation, r_{ij} , results from a pairwise comparison of two data pairs, i.e. x_i and x_j , where the strength of the relationship between data sample x_i and data sample x_i is defined according to Eq. (6):

$$r_{ij} = \frac{\left|\sum_{k=1}^{m} x_{ik} x_{jk}\right|}{\sqrt{\left(\sum_{k=1}^{m} x_{ik}^{2}\right)\left(\sum_{k=1}^{m} x_{jk}^{2}\right)}}$$
(6)

Where:

 r_{ij} = strength values of relations between input variables and output parameters, and

 $i, j = 1, 2, \ldots, n.$

According to Eq. (6) this method is related to the dot product for the cosine function. When two vectors are collinear (most similar), dot product will be unity; when the two vectors are perpendicular to each other (most dissimilar), dot product will be zero [61].

Figs. 10–17 show the strength values of relations (r_{ij}) between input variables (t, H, K, E, θ) and output parameters.

As can be seen from these figures, effectiveness of all input variables have nearly same values. Nevertheless, for all output parameters, overburden of buried tunnel (H) is the most effective parameter than other four input variable, and θ value (position of key segment) has the least effect on output parameters.

8 Model performance

Performance of each ANN model must be calculated in predicting ability of output values. To do this, four performance indices including coefficient of determination (R^2) , proportion of variance explained (PVE) or variance accounted for (VAF), coefficient of efficiency (CE) and root mean squared error (RMSE) were selected and calculated based on testing data sets. These data sets selected randomly from database and not included in the model training. VAF and CE values are calculated using Eq. (7) and Eq. (8):

$$VAF = 100 \times \left(1 - \frac{\operatorname{var}\left(u_{k} - \hat{u}_{k}\right)}{\operatorname{var}\left(u_{k}\right)}\right)$$
(7)

$$CE = 1 - \frac{\sum_{k=1}^{N} (\hat{u}_{k} - u_{k})^{2}}{\sum_{k=1}^{N} (\hat{u}_{k} - \overline{\hat{u}_{k}})^{2}}$$
(8)

Where:

var is the variance; \hat{u}_k and u_k are the k_{th} predicted and measured values respectively;

 $\overline{\hat{u}}_{i}$ is the average of predicted values; and N is the number of data.

VAF index express the degree of difference between the variances of measured and predicted data sets. The values of VAF closer to 100 % indicate low variability and consequently better prediction capabilities. The lower the RMSE, the better the model performs [62, 63]. In ideal condition, the value of RMSE should be zero and value of CE should be unity. Obtained values for these indices are presented in Table 6. Also the graphs of correlation coefficient (R^2) for each type of input data (all data, training, test and validation) for output parameters are presented in Figs. 18-25. Relationship between output and target values for each type of input data and each output parameter are presented next to the related graphs. Obtained results show that minimum value of correlation coefficient relates to the minimum displacement of the ring (Fig. 25). However all obtained values show that generally high correlation is governed between all output and target values.













Fig. 13 Sensitivity analysis of minimum Tresca stress

Table of renormance indices of the network model										
Performance Index	Output parameters									
	MisesMax	MisesMin	TrescaMax	TrescaMin	MaxPrinMax	MinPrinMin	UMax	UMin		
RMSE (%)	3	6	4	4	5	3	5	5		
R2 (%)	98	95	98	98	97	99	97	93		
VAF (%)	98	95	98	98	97	99	97	93		
CE	97	95	98	98	97	99	97	93		

Table 6 Performance indices of the neural network model	
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Stress Analysis of Segmental Tunnel Lining Using Artificial Neural Network









Fig. 15 Sensitivity analysis of minimum principal stress



Fig. 16 Sensitivity analysis of maximum displacement



Fig. 17 Sensitivity analysis of minimum displacement



Fig. 18 Correlation coefficient for maximum Mises stress



Fig. 19 Correlation coefficient for minimum Mises stress



Fig. 20 Correlation coefficient for maximum Tresca stress



Fig. 21 Correlation coefficient for minimum Tresca stress



Fig. 22 Correlation coefficient for Maximum value of maximum Principal stress



Fig. 23 Correlation coefficient for Minimum value of minimum Principal stress



Fig. 24 Correlation coefficient for Maximum displacement



Fig. 25 Correlation coefficient for Minimum displacement

9 Conclusions

To achieve knowledge about the safety of the support system of tunnel lining ring, von Mises and Tresca stresses together with principal stresses and extreme values of ring displacements were determined using finite element method. A segmental tunnel lining ring with 5+1 segments is modelled. To prepare enough data for ANN, parametric analysis was done. 252 numerical models were solved. After preparation of sufficient required input data, multi-layer perceptron neural net was selected as prediction model. Firstly, number of neurons and their arrangement in two hidden layers were optimized based on minimum obtained values for RMSE from input data variables. The minimum value of RMSE was 0.05 for 11 number of neurons. This obtained value for number of neurons in hidden layers was in conformity with the presented relations in literature. Consequently, in 5-7-4-1 structure arrangement of neural net model, resulted minimum value for RMSE was 0.041 and 0.055 for transfer functions of TANSIG and LOGSIG, respectively. Then the model tested and validated using different datasets. Sensitivity analyses were performed to determine the influence of each input variable on different types of output parameters. The obtained results were as below:

- Although sensitivity analysis showed that all the input variables have nearly same value of influence on the output parameters, but in all conditions, Height (H) and θ input variables are the most and less effective parameters on outputs parameters than three other input variables, respectively.
- Also the performance of presented model was evaluated using RMSE, R², VAF and CE indices. Obtained results showed the excellent ability of the presented model in prediction of different type of stresses and extreme values of ring displacement and this prediction model can be used in high accuracy to obtain reliable results for preliminary study and design of segmental tunnel lining instead of current time consuming and expensive methods.

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