FINITE ELEMENT METHOD FOR THE COMPUTATION OF THE ELECTROMAGNETIC FIELD OF WAVEGUIDES

I. Vágó

Department of Electromagnetic Theory, Technical University, H-1521 Budapest

Received June 5, 1986

Abstract

The electromagnetic field of waveguides is customarily derived from an electric or magnetic vector potential. A functional may be written for the potentials which attains extrem value if the vector potentials satisfy the wave equation. The studied region is subdivided into triangles within which linear approximation is employed. In the present case the integral in the functional can be written in an analytical form. Having sought the extremum and taking the different boundary conditions of TM and TE modes into account, a set of linear equations is obtained. The unknowns are the nodal vector potential values. The set is solved by computer, and the method is illustrated by examples.

The electromagnetic field of waveguides is usually derived with the aid of an electric or magnetic vector potential A^{em} . With the axis of the waveguide chosen as the z axis, the z-directed vector potential can be written in Cartesian coordinates in the product form

$$A = \Theta(x, y)e^{-\gamma z} \tag{1}$$

where the term $e^{-\gamma z}$ describes the variation in the z-direction and γ is the propagation coefficient in the z-direction. Θ depends upon the transversal coordinates only. In case of harmonic time-variation Θ satisfies the wave equation

$$\Delta \Theta + k^2 \Theta = 0 \tag{2}$$

where k^2 and γ^2 are related as

$$k^2 = \gamma^2 + \omega^2 \mu \varepsilon. \tag{3}$$

Eq. (2) can also be obtained by equating the first variation of the functional

$$I = \int_{S} (\operatorname{grad}^{2} \Theta - k^{2} \Theta^{2}) dS \tag{4}$$

with zero. Here S denotes the cross section of the waveguide in the transversal plane and the gradient should be taken with respect to the transversal

coordinates. The functional (4) may attain an extremal value, if its first variation vanishes i.e.

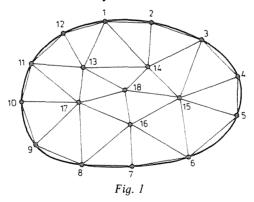
$$\delta I = -2 \int_{S} \eta (\Delta \Theta + k^2 \Theta) dS - \oint_{l} \eta \frac{\partial \Theta}{\partial n} dl = 0$$
⁽⁵⁾

where *l* is the curve bounding the cross section *S* and $\frac{\partial \Theta}{\partial n}$ is the derivative of Θ with respect to the outer normal.

The function $\eta(x, y)$ appearing here is continuous in S along with its first two derivatives and, in case of Dirichlet boundary conditions, it vanishes on l, otherwise it is arbitrary.

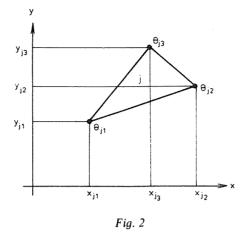
Eq. (5) may hold only if both the surface and line integrals are zero. The surface integral equals zero irrespective of the choice of η , if Eq. (2) is satisfied. The line integral is zero at Dirichlet boundary conditions since then $\eta = 0$ on l, whereas at homogeneous Neumann boundary conditions it vanishes because then $\frac{\partial \Theta}{\partial n} = 0$ on l. It is thus evident from Eq. (5) that the homogeneous Neumann boundary condition of the functional (4).

The integral (4) can be approximately written with the aid of the finite element method. To this end the region S is divided into m triangles with the aid of nodes selected on the boundary and in the interior of the region and the



curve *l* is approximated by a curve formed by the relevant triangle edges (Fig. 1). The triangles and their nodes are given order numbers. The global order numbers of the nodes on the curve *l* are $1, 2, ..., n_1$, and those for the nodes inside the region are $n_1 + 1, n_1 + 2, ..., n$. The three nodes of the *j*th triangle are also assigned local order numbers: j_1, j_2, j_3 (Fig. 2). The function $\Theta(x, y)$ is approximated in the *j*th triangle by the linear function

$$\Theta(x, y) = a_{j0} + a_{j1}x + a_{j2}y, \tag{6}$$



the values Θ_i (i=1, 2..., n) corresponding to the nodes of the triangular subregions are regarded as unknowns and the column matrix formed by these is denoted by Θ_0 . A column matrix is also formed by the values Θ_j , corresponding to the nodes of the *j*th triangle and this is denoted by Θ_j . Θ_j can be expressed with the aid of Θ_0 as

$$\boldsymbol{\Theta}_{i} = \boldsymbol{G}_{i} \,\boldsymbol{\Theta}_{0}. \tag{7}$$

The three rows of G_j correspond to the nodes of the *j*th triangle, and its columns to the nodes $1, 2, \ldots, n$ selected in the region S. The *k*th element in the *i*th row of G_j is 1, if the global order number of the node *j*, in the *j*th triangle is *k*, otherwise the element is zero.

If the coordinates of the nodes of the *j*th triangle are $(x_{j1}, y_{j1}), (x_{j2}, y_{j2}), (x_{j3}, y_{j3})$ then according to (6)

$$\boldsymbol{\Theta}_{j} = \begin{bmatrix} 1 & x_{j1} & y_{j1} \\ 1 & x_{j2} & y_{j2} \\ 1 & x_{j3} & y_{j3} \end{bmatrix} \begin{bmatrix} a_{j0} \\ a_{j1} \\ a_{j2} \end{bmatrix}$$
(8)

Hence

grad
$$\Theta_{j} = \begin{bmatrix} a_{j1} \\ a_{j2} \end{bmatrix} = \frac{1}{D_{j}} \begin{bmatrix} y_{j2} - y_{j3} & y_{j3} - y_{j1} & y_{j1} - y_{j2} \\ x_{j3} - x_{j2} & x_{j1} - x_{j3} & x_{j2} - x_{j1} \end{bmatrix} \Theta_{j} = F_{j} \Theta_{j}$$
(9)

where

$$D_{j} = (x_{j2} - x_{j1})(y_{j3} - y_{j2}) - (x_{j3} - x_{j1})(y_{j2} - y_{j1}).$$
(10)

I. VÁGÖ

Substituting (7) into (9)

$$\operatorname{grad} \Theta_j = F_j G_j \Theta_0 = H_j \Theta_0. \tag{11}$$

Its square is

$$\operatorname{grad}^{2} \Theta_{j} = \Theta_{0}^{T} H_{j}^{T} H_{j} \Theta_{0}$$
(12)

where Θ_0^T and H_j^T are obtained by transposing Θ_0 and H_j . Since grad² Θ_j is constant in the *j*th triangle, its integral over the triangle equals its product with the area S_j . So the first term on the right hand side of (4) can be approximately written as

$$I_1 = \int_{S} \operatorname{grad}^2 \Theta \, dS \approx \Theta_0^T \sum_{j=1}^m S_j H_j^T H_j \Theta_0.$$
⁽¹³⁾

The part over the *j*th triangle in the second term of the integral (4) can be expressed with the aid of the values Θ_{j1} , Θ_{j2} , Θ_{j3} of Θ assumed in the nodes of the *j*th triangle if Θ_i varies as in Eq. (6) (Fig. 2).:

$$I_{2j} = -\int_{S} k^{2} \Theta_{j2} dS = -k^{2} \frac{S_{j}}{6} (\Theta_{j1}^{2} + \Theta_{j2}^{2} + \Theta_{j3}^{2} + \Theta_{j1} \Theta_{j2} + \Theta_{j2} \Theta_{j3} + \Theta_{j3} \Theta_{j1}).$$
(14)

Introducing the notation

$$\mathbf{R} = \begin{bmatrix} 1 & \frac{1}{2} & \frac{1}{2} \\ \frac{1}{2} & 1 & \frac{1}{2} \\ \frac{1}{2} & \frac{1}{2} & 1 \end{bmatrix}$$
(15)

[6] and using Eq. (7)

$$I_{2j} = -k^2 \frac{S_j}{6} \Theta_j^T R \Theta_j = -k^2 \frac{S_j}{6} \Theta_0^T G_j^T R G_j \Theta_0.$$
⁽¹⁶⁾

Over the cross section S:

$$I_{2} = -\int_{S} k^{2} \Theta^{2} dS \approx \sum_{j=1}^{m} I_{2j} =$$
$$= -\frac{k^{2}}{6} \Theta_{0}^{T} \sum_{j=1}^{m} S_{j} G_{j}^{T} R G_{j} \Theta_{0}.$$
(17)

According to Eqs. (13) and (17) the functional (4) can be approximated as

$$I = I_1 + I_2 \approx \Theta_0^T \sum_{j=1}^m S_j \left[H_j^T H_j - \frac{k^2}{6} G_j^T R G_j \right] \Theta_0.$$
(18)

Introducing the notations

$$\boldsymbol{P} = \sum_{j=1}^{m} S_j \boldsymbol{H}_j^T \boldsymbol{H}_j, \tag{19}$$

$$\boldsymbol{Q} = -\frac{1}{6} \sum_{j=1}^{m} S_j \boldsymbol{G}_j^T \boldsymbol{R} \boldsymbol{G}_j$$
(20)

the formula

$$I \approx \Theta_0^T (\boldsymbol{P} - k^2 \boldsymbol{Q}) \Theta_0 \tag{21}$$

is obtained.

In the following the TE mode solution is first discussed and thereafter the TM one is treated.

In case of TE mode the electric vector potential A^e namely its term Θ depending upon the transversal coordinates satisfies homogeneous Neumann boundary condition on the boundary which is a natural boundary condition of the variational problem. (21) may be extremal if

$$\frac{\partial I}{\partial \Theta_0} = 2(\boldsymbol{P} - k^2 \boldsymbol{Q}) \Theta_0 = 0.$$
(22)

This set of homogeneous linear equations may have nontrivial solution only if

$$\det | \boldsymbol{P} - k^2 \boldsymbol{Q} | = 0 \tag{23}$$

i.e. if k^2 is an eigenvalue of the matrix $Q^{-1}P$. Different TE mode solutions correspond to the different eigenvalues with their propagation coefficients obtainable from Eq. (3). Each of the values k^2 at a particular mode involves an eigenvector Θ_0 . Its elements are the approximate values of Θ in the nodes.

In case of TM mode the term Θ of the magnetic vector potential A^m satisfies homogeneous Dirichlet boundary condition on the boundary of the region S, i.e. Θ vanishes everywhere on the boundary. Hence the first n_1 elements of the column vector Θ_0 are zero, so Θ_0 can be partitioned as follows

$$\boldsymbol{\Theta}_{0} = \begin{bmatrix} \boldsymbol{\Theta}_{01} \\ \boldsymbol{\Theta}_{02} \end{bmatrix} = \begin{bmatrix} \boldsymbol{0} \\ \boldsymbol{\Theta}_{02} \end{bmatrix}.$$
(24)

Let the matrices P and Q also be partitioned to make P_{11} and Q_{11} square submatrices of order n_1 . Thus from Eq. (21)

$$I \approx \begin{bmatrix} \Theta_{01}^T & \Theta_{02}^T \end{bmatrix} \left\{ \begin{bmatrix} P_{11} & P_{12} \\ P_{21} & P_{22} \end{bmatrix} + k^2 \begin{bmatrix} Q_{11} & Q_{12} \\ Q_{21} & Q_{22} \end{bmatrix} \right\} \begin{bmatrix} \Theta_{01} \\ \Theta_{02} \end{bmatrix}$$
(25)

Hence, taking $\Theta_{01} = 0$ into account

$$I \approx \Theta_{02}^T [\boldsymbol{P}_{22} - k^2 \boldsymbol{Q}_{22}] \Theta_{02}.$$

This may be extremal if

$$\frac{\partial I}{\partial \boldsymbol{\Theta}_{02}} = 2[\boldsymbol{P}_{22} - k^2 \boldsymbol{Q}_{22}]\boldsymbol{\Theta}_{02} = \boldsymbol{0}$$
(27)

Now, the values of k^2 are the solutions of the equation

$$\det | \boldsymbol{P}_{22} - k^2 \boldsymbol{Q}_{22} | = 0.$$
 (28)

The elements of the eigenvectors Θ_{02} corresponding to the eigenvalues k^2 are approximations of the values of Θ in the internal nodes.

A computer program has been developed based on the method presented. With this, several cross sections have been treated to obtain the values k^2 and wavelengths λ corresponding to different modes, and to plot the electrical flux density lines of TE modes and the magnetic flux density lines of TM modes.

To test the method a rectangular cross section waveguide has been first examined (Fig. 3). The exact values and the finite element approximations of the wavelengths are summarized in Table 1. The flux plots for a quarter of the cross section have been plotted in Fig. 3.

As a second example the cross section shown in Fig. 4 has been treated. For this case the results obtained by the method of finite differences for the fundamental TM mode are given in reference [5]. The wavelengths and the flux plots are shown in Fig. 4.

Flux plots obtained for an elliptical cross section waveguide are shown in Fig. 5.

m	n	TE mode			TM mode		
		λ_e/cm exact	λ _a /cm approx	$\frac{\lambda_a - \lambda_e}{\lambda_e} 100$	λ_e/cm exact	λ _a /cm approx	$\frac{\lambda_a - \lambda_e}{\lambda_e} 100$
0	1	3.60	3.59	-0.27			
1	0	4.80	4.79	-0.27			
1	1	2.88	2.86	-0.82	2.88	2.86	-0.89
2	1	2.00	1.96	-1.89	2.00	1.96	-0.49
1	2	1.69	1.66	-1.70	1.69	1.66	-1.70
2	0	2.40	2.37	- 1.09			
0	2	1.80	1.78	-1.06			
2	2	1.44	1.41	-1.82	1.44	1.41	-1.82



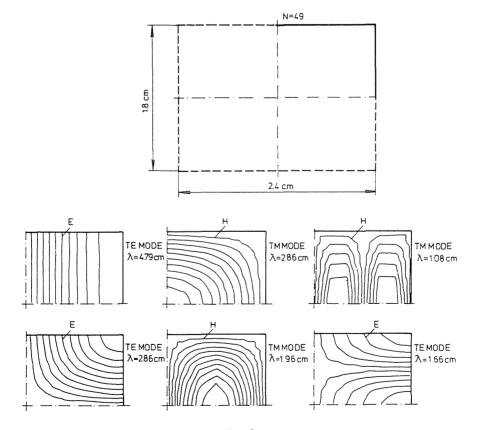


Fig. 3

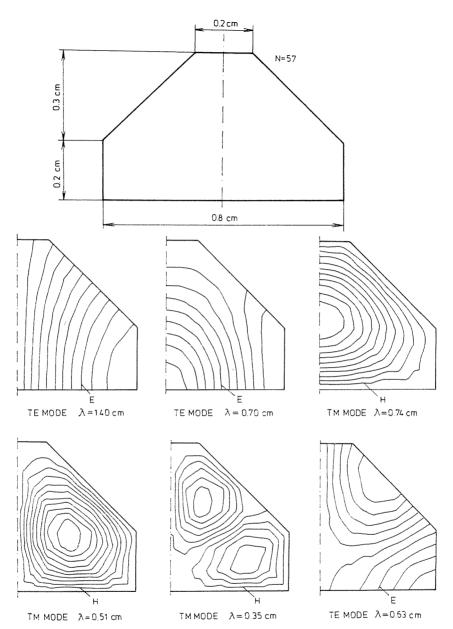


Fig. 4

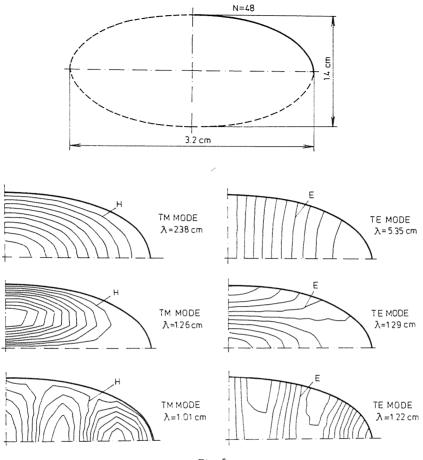


Fig. 5

References

- 1. PREIS, K.: Anwendung der Methode der finiten Elemente zur numerischen Berechnungen elektromagnetischer Felder, Habilitationsschrift, Graz, 1983.
- 2. ARLETT, P. L. et al.: Application of finite elements to the solution of Helmholtz's equation, Proc. IEE, Vol. 115, No. 12, Dec. 1968.
- CSENDES, Z. J.-SILVESTER, P.: Numerical solution of dielectric loaded waveguides. I-Finiteelement analysis, IEEE Trans. MTT-18, No. 12 (1970).
- 4. LARSEN, T.: On the relation between modes in rectangular, elliptical and parabolic waveguides and a mode-classifying system, IEEE Trans. MTT-20, No. 6 (1972).
- 5. GOVORKOV, V. A.: Electric and magnetic fields, Energiya, Moscow, 1960 (in Russian).
- 6. AHMED, S.-DALY, P.: Waveguide solutions by the finite-element method. The Radio and Electronic Engineer, Vol. 18., 217-223 (1969).

Prof. Dr. István VÁGÓ H-1521 Budapest

3 Periodica Polytechnica Electrical Eng. 31/1 - 2