

Fault Tolerant Power Converter Topologies for Sensor-less Speed Control of PMSM Drives

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Abstract

This paper exhibits a sensor-less speed control method based MRAS observer applied to a fault-tolerant PMSM drive system. So, this paper proposes a rapid method of fault switch detection in the power converters aiming to make sure the continuity of service even though the fault presence of an opening phase. In fact, the MRAS observer is used to replace the mechanical sensor and a redundant inverter leg is equally employed to replace the faulty leg. The proposed fast fault diagnosis method has the features of simple algorithm, independence of the transient states and being simply integrated without any additional sensors.

Keywords

Permanent Magnet Synchronous Machine (PMSM), Direct Torque Control (DTC-SVM), FTC, MRAS

1 Introduction

Actually, the permanent magnet synchronous motors (PMSM) are efficiently applied to various applications as the electric vehicles, the aerospace industry, the medical service and the military applications thanks to several outstanding characteristics. However, the human life damages and the cost will become definitely serious, if a failure of the drive system takes place in these applications. It is evidence because of the importance of high reliable operation in these areas. Subsequently, it is an urgent need to search a fault control to improve the electrical motor performances [1-3]. In the literature, the multitudes of control solutions for PMSM have already been investigated accordingly. The DTC-SVM controls are so powerful; they are insensitive to parameters changes of the machines and robust against to the disturbance. They are even able to reduce the ripples of the flux and the torque compared to the classical DTC [4-6].

Indeed, the main objective of this DTC-SVM technique is to make a controller of stator flux vector in a fixed (α, β) reference. Afterwards, the polar forms of these two vectors are achieved only through their projections on the reference frame (α, β) . Hence, the desired increment of the stator flux vector at a given time is calculated out of these components.

Additionally, a sensor-less control with MRAS is introduced so as to reduce the hardware complexity and the size of the drives as well. Furthermore, it rules out the sensor cable, enhances the reliability and decreases the maintenance requirements [7-9].

In the literature, statistic results show that about 40 % of the failures in variable speed ac drives in industrial systems are concentrated in power electronics. Sometimes, if no redundant equipment is already available, a rapid shutdown of the industrial systems has occurred. This stop is accompanied by the loss of production and an unavoidable cost of repair. Consequently, given the importance of power converter safety operation in several fields such as electric traction, renewable energy and so forth it is necessary to examine availability of these industrial systems in the case of shutdown of an IGBT module, a converter leg or a phase machine. Thus, this paper proposes a novel fault diagnosis approach allows the PMSM drive of operating after fault occurrence. The proposed approach is advantageous in that it does not require additional sensors, complex hardware or complex calculations.

2 PMSM Model

The d - q axis stator flux linkages in the synchronous reference frame can be expressed as follows:

$$\Phi_d = L_d i_d + K_e \tag{1}$$

$$\Phi_q = L_q i_q. \tag{2}$$

The d - q axis voltage equations in the synchronous reference frame may be expressed as:

$$v_d = R_s i_d + L_d \frac{di_d}{dt} - \omega_r L_q i_q \tag{3}$$

$$v_q = R_s i_q + L_q \frac{di_q}{dt} + \omega_r (L_d i_d + K_e) \tag{4}$$

where $K_e = \sqrt{\frac{3}{2}} \Phi_m$.

Using Eqs. (1) and (2), electromagnetic torque is given by

$$T_e = \frac{3}{2} p (K_e i_q + (L_d - L_q) i_d i_q) \tag{5}$$

$$\frac{di_d}{dt} = \frac{R_s}{L_d} i_d + \frac{L_q}{L_d} \omega_r i_q + \frac{v_d}{L_d} \tag{6}$$

$$\frac{di_q}{dt} = -\frac{R_s}{L_q} i_q - \frac{L_d}{L_q} \omega_r i_q - \frac{K_e}{L_q} \omega_r + \frac{v_q}{L_q} \tag{7}$$

$$\frac{d\omega_r}{dt} = -p^2 \left(\frac{L_d - L_q}{J} \right) i_d + p^2 \frac{K_e}{J} i_q - \frac{f}{J} \omega_r + p \frac{T_l}{J}. \tag{8}$$

3 Fault tolerant inverter (FTI)

Fig. 1 shows mainly a three-phase standard six-switch inverter, enriched by with three fuses and three TRIACs. In healthy mode, the structure of the presented DTC-SVM fault tolerant inverter is equally the same as a standard three-phase six switches inverter. The adopted inverter fault tolerant control has the objective to accommodate the opening of a phase fault or a short circuit. Subsequently, we considered only the open phase fault (phase A) case in this paper. Similarly, the same procedure is applied to the phase B and phase C.

Moreover, Fig. 2 displays the new inverter topology, after a fast detection and an isolation of the open phase (phase A) [7]. In this paper, we studied two cases successively: the healthy and the faulty modes.

In this paper a methodology for isolating the faulty switching device was proposed where the phase with a faulty switch is isolated and connected to the midpoint of

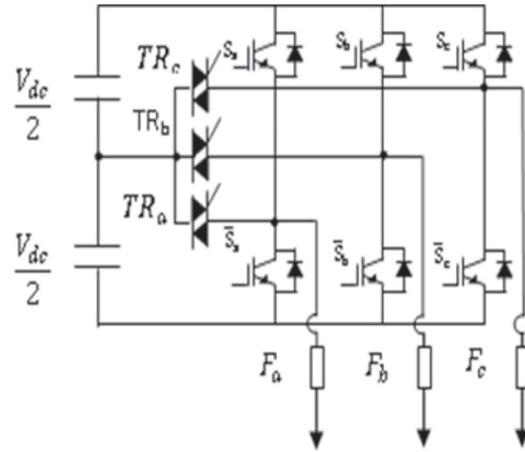


Fig. 1 Healthy mode inverter

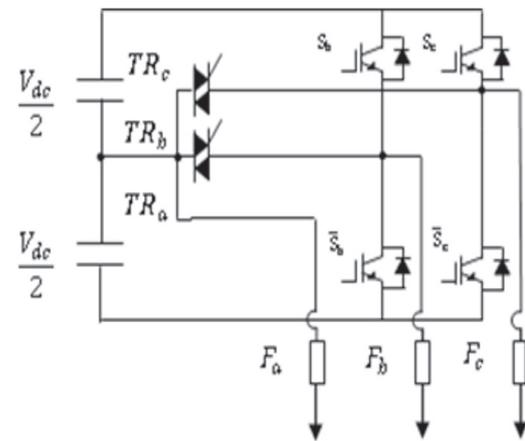


Fig. 2 Fault tolerant inverter fed PMSM drive

DC link. During the post-fault operation three phase currents are still shifted by 120 electrical degrees as in the normal healthy operation. During the post-fault operation the voltage applied to the machine terminals is reduced. However, since all three phases contribute to torque production under fault condition the current rating in this case for producing the rated torque is the same as that in the healthy condition. Consequently, the size and rate of the IGBT switches remain the same as the standard inverter.

4 Model reference adaptive system

During the operation of an electrical machine, the parameters can be easily changed and its performance decreases remarkably. As consequence, the MRAS can resolve this problem as it (The Model Reference Adaptive System (MRAS)) is a significant observer [10-13]. Relying on the Eqs. (6) and (7), the state model is the stator current that is chosen as a variable state is:

$$\begin{bmatrix} \frac{di_d}{dt} \\ \frac{di_q}{dt} \end{bmatrix} = \begin{bmatrix} -\frac{R_s}{L_d} & \frac{L_q}{L_d} \omega_r \\ -\frac{L_d}{L_q} \omega_r & -\frac{R_s}{L_q} \end{bmatrix} \begin{bmatrix} i_d \\ i_q \end{bmatrix} + \begin{bmatrix} \frac{V_d}{L_d} \\ \frac{V_q}{L_q} - \frac{K_e}{L_q} \omega_r \end{bmatrix} \quad (9)$$

where

$$i_d^* = i_d + \frac{K_e}{L_d}, \quad i_q^* = i_q \quad (10)$$

$$V_d^* = V_d + \frac{K_e}{L_d} R_s, \quad V_q^* = V_q. \quad (11)$$

According to the general structure of the adaptation law, the $\hat{\omega}_r$; can be expressed in the form of Eq. (12).

$$\hat{\omega}_r = \int_0^t \psi_1(v, \tau) d\tau + \psi_2(v, t) + \hat{\omega}_r(0) \quad (12)$$

Where v is the output of the block. ψ_1 and ψ_2 area as follow.

$$\begin{cases} \psi_1(v, t) = K_1 e^T L \hat{i}^* \\ \psi_2(v, t) = K_2 e^T L \hat{i}^* \end{cases} \quad (13)$$

where

$$L = \begin{bmatrix} 0 & \frac{L_q}{L_d} \\ -\frac{L_d}{L_q} & 0 \end{bmatrix}, \quad e = \begin{bmatrix} i_d^* - \hat{i}_d^* \\ i_q^* - \hat{i}_q^* \end{bmatrix}, \quad \hat{i}^* = \begin{bmatrix} \hat{i}_d^* \\ \hat{i}_q^* \end{bmatrix}. \quad (14)$$

The estimation speed is as following

$$\hat{\omega} = \left(K_p + \frac{K_i}{p} \right) \left[\frac{L_q}{L_d} i_d \hat{i}_q - \frac{L_d}{L_q} \hat{i}_d i_q - \frac{K_e}{L_q} (i_q - \hat{i}_q) + \hat{i}_d \hat{i}_q \left(\frac{L_d}{L_q} - \frac{L_q}{L_d} \right) \right] + \hat{\omega}(0). \quad (15)$$

Relying on Eqs. (14) and (15), the block diagram control of the PMSM is based on MRAS can be obtained in Fig. 3.

5 Direct torque control space vector modulation

The DTC-SVM improves greatly the torque and the flux performance through the achieved and the fixed switching frequency and the decreased torque and the flux ripples as well.

$$T_e = \frac{3}{2} n_p \left[\frac{|\Phi_s| K_e \sin \delta}{L_d} - \frac{|\Phi_s|^2 (L_q - L_d) \sin(2\delta)}{2L_d L_q} \right] \quad (16)$$

From the Eq. (16), we can see that the constant stator flux amplitude $|\Phi_s|$ and the flux produced by permanent magnet K_e , the electromagnetic torque can be changed by the control of the torque angle δ . If the stator resistance is neglected, the torque angle is between the stator and rotor flux linkage.

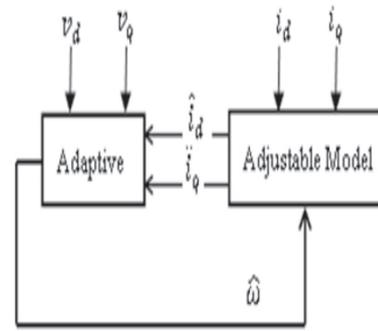


Fig. 3 The block diagram control of the PMSM is based on MRAS

The torque angle by the way can be replaced just by changing the position of the stator flux vector θ_e in respect to PM vector using the actual voltage vector supplied by PWM inverter. In the steady state, δ is constant and corresponds to a load torque whereas stator and rotor flux rotate at synchronous speed. In transient operation, δ varies and the stator and rotor flux rotate at different speeds (Fig. 4).

The relationship between the torque error and the increment of the load angle δ is a nonlinear. Therefore, we use PI controller that generates the load angle increment required to minimize the instantaneous error between the reference T_{e_ref} and the actual T_e torque.

Thereby, the torque error signal ΔT_e is delivered to the PI controller, which determines the increment of the torque angle δ . Relying on this signal and reference amplitude of stator flux Φ_{e_ref} , the reference voltage vector in stator coordinates α, β is determined. In addition, the calculation block of the reference voltage vector also uses data about the actual stator flux vector (amplitude Φ_s and position θ_s) as well as the measured current vector I_s . Hence, the reference stator voltage vector is delivered to the space vector modulator (SVM) which generates the switching signals S_a, S_b and S_c for the power transistors of inverter. As well as, the calculation block of reference voltage vector is shown in Fig. 5.

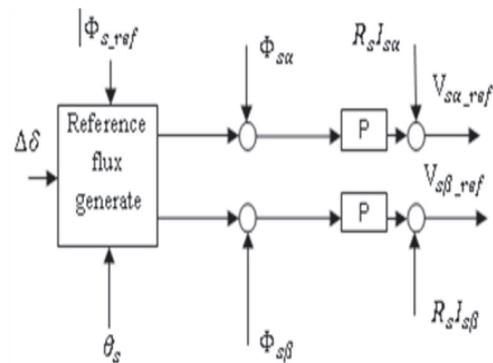


Fig. 4 Calculation block of the reference voltage vector

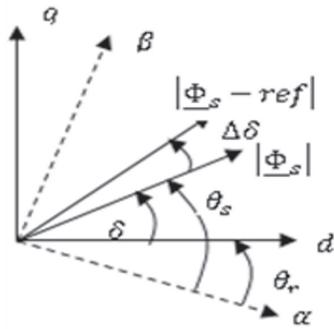


Fig. 5 Space Vector Diagram illustrating Torque Control Conditions

Depending on the $\Delta\delta$ signal, the reference of stator flux amplitude to $\Delta\delta$ signal, the reference of stator flux amplitude $|\Phi_{s-ref}|$, the measured stator flux vector position θ_s (Fig. 5) the reference flux components Φ_{sa-ref} , Φ_{sb-ref} in stator coordinate system are calculated as:

$$\begin{cases} \Phi_{sa-ref} = |\Phi_{s-ref}| \cos(\theta_s + \Delta\delta) \\ \Phi_{sb-ref} = |\Phi_{s-ref}| \sin(\theta_s + \Delta\delta) \end{cases} \quad (17)$$

For a constant flux operation region, the reference value of stator flux amplitude $|\Phi_{s-ref}|$ is equal to flux amplitude of permanent magnet K_e .

The command voltage can be determined from the flux errors in α, β coordinate system as following.

$$\begin{cases} v_{sa-ref} = \frac{\Delta\Phi_{sa}}{T_s} + R_s I_{sa} \\ v_{sb-ref} = \frac{\Delta\Phi_{sb}}{T_s} + R_s I_{sb} \end{cases} \quad (18)$$

Where T_s is the sampling time, $\Delta\Phi_{sa} = \Phi_{sa-ref} - \Phi_{sa}$ and $\Delta\Phi_{sb} = \Phi_{sb-ref} - \Phi_{sb}$.

The structure of the proposed control schema, which is presented in this paper is shown in the Fig. 6.

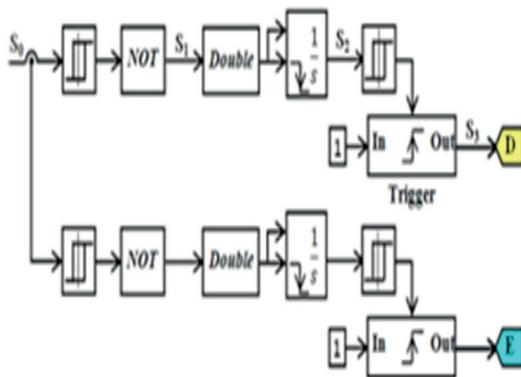


Fig. 6 Fault Detection Isolation Algorithm (FDI)

6 Fault tolerant control

The design and the modeling of some faults types in the electric actuators and particularly in the inverter faults (component faults) are very important tasks. Subsequently, the development of the control strategy is able to detect, to isolate and to ensure the continuity of functioning of the system, which becomes a necessity. Many studies have been already conducted to detect an electrical fault in the machine, in the inverter and in the power circuits. Hence, each fault generates one or more perturbations. Therefore, the detection out of that should be traceable to the fault. The choice and the desired signature extraction method differ from one technique to another. The open circuit faults are identifiable from their observed measuring currents and lead to a current decrease as a result (or voltage) on the faulty phase signatures.

If the abnormal operation is detected, the fault is localized with some specific test loop at each leg inverter, which allows knowing the IGBT module where the fault occurred. Fig. 6 shows the applied technique (series of tests) for fault detection and localization using the same operations and signal generation for the intervention of these fault tolerant control [14-16].

S0: Represents the signal of the measured current on phase a. (the same thing for a and c phase)

D, E: Represents the signal (1or 0 logic) to control signal of triacTRa.

The schematic diagram for generating the control signals of triacs is given by Fig. 7. Using the two signals generated by the FDI algorithm, for example, the control signal of triacTRa is set to 1. The triacTRa is used to connect the redundant leg.

The performance of system after fault occurrence in TRIACs is similar to the one-phase open-circuit fault.

When this fault occurs, during the faulty mode only the faulty phase current become zero while the healthy phase have increased magnitudes.

After the fault occurrence, the ripples of the torque are bigger than that under the safe inverter. This fault may also produce a small real speed ripples. Consequently, the

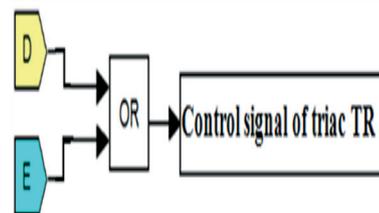


Fig. 7 Schematic diagram for generating the control signals of triacs

fault conditions cause abnormal rotor vibrations and give abnormalities in the drive’s operation.

The reconfiguration of drive system can be realized by acting on its control algorithm of this type of fault.

7 Simulation results

7.1 Healthy mode

The simulation results of the proposed control, previously discussed under the inverter fault has been carried out with the scheme block Fig. 8 relying on Matlab/Simulink. The drive system is composed of a PMSM (parameters are listed in Table 1) and a fault tolerant inverter as shown in Fig. 1.

7.2 Open phase faulty mode

After the fault occurrence, the ripples of the torque are bigger than that under the safe inverter. This fault may also produce a small real speed ripples. Consequently, the fault conditions cause abnormal rotor vibrations and give abnormalities in the drive’s operation. Simulation results of the line currents (i_a , i_b and i_c). As from the occurrence of fault at $t = 0.75$ s, the magnitude of stator currents increases, the current i_a becomes zero, while i_b and i_c undergo a slight deformation.

7.3 Fault tolerant control

The capacitors in the DC-link are really assumed to be infinite so that the voltage on both capacitors is constant and equal to $\frac{V_{dc}}{2}$.

In the first test, Fig. 9 shows a typical start-up of the PMSM with no fault. The reference rotor speed is set up at 1500 rpm with a nominal load torque step $T_l = 4$ Nm applied to the system at time $t = 0.4$ s. As Fig. 8 displays that the speed drop at the time of applying a load torque does not exceed 4 %, the duration of the disturbance does not exceed 0.6 s. While Fig. 10 exhibits additionally the waveforms of the electromagnetic torque, Fig. 11 illustrates the waveforms of the currents i_a .

In the second test, the PMSM started without load torque and then a nominal load torque is applied at 0.4 s.

An open phase fault is created by a cutting of motor power phase. Consequently, the open phase fault of the PMSM introduced an unbalance in the stator winding currents. Like it’s shown in the Fig. 12, the machine continues to rotate with oscillations as a consequence of the huge oscillations in the torque. Finally, faults in IGBTs generally do not cause system shutdown, but degrade its performances. The Fig. 13 shows the rotor speed, Fig. 14 the stator currents, Fig. 12 the electromagnetic of the PMSM

Table 1 PMSM Parameters

Parameters		Specification	
R_s	0.5 Ω	Rated power	1.570 kW
L_d	3.9 mH	Rated voltage	400 V
L_q	3.7 mH	Rated current	5.9 A
K_t	0.910 Nm/A	Vdc	540 V
K_e	0.2275 V.s/rad	Number of pole pairs	4
J	$5.8 \cdot 10^{-4}$ Kg.m ²	Rated speed	3000 rpm
f	0.00374 Nm./rad	Rated torque	5 Nm

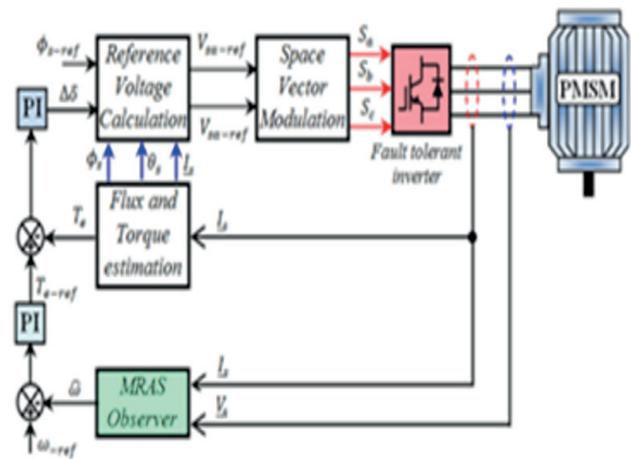


Fig. 8 SVM based DTC control scheme for PMSM

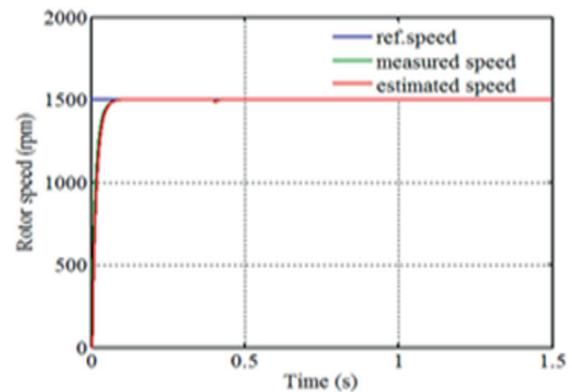


Fig. 9 Waveform of speed

to an open phase fault. As shown prior in the Fig. 10, the machine keeps rotating enormously with huge oscillations in the torque. In FTC mode, after having shown that the system does not able to function in case of a failure, this section shows results of the inverter reconfiguration; Fig. 17 shows the simulation results under the same conditions (the reference rotor speed is set at 1500 rpm with a nominal load torque step $T_l = 4$ Nm) relying on an open phase. However, we note a presence of disturbances in the amplitudes of the currents at the time of fault and the removal of the positive alternating of i_a current which

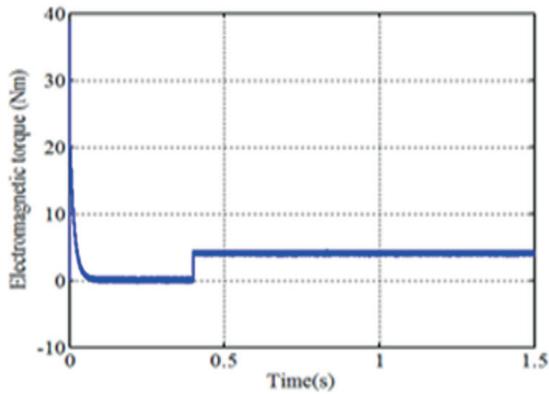


Fig. 10 Waveform of electromagnetic torque

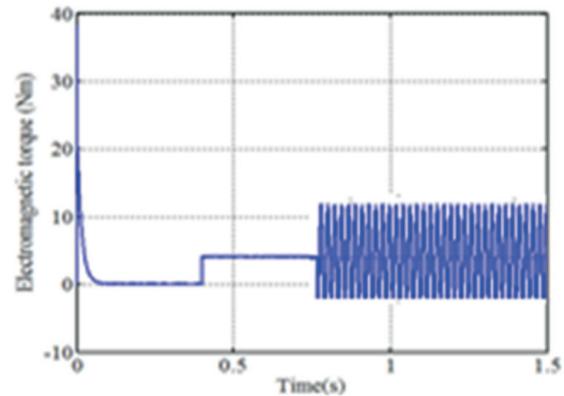


Fig. 13 Waveform of the speed

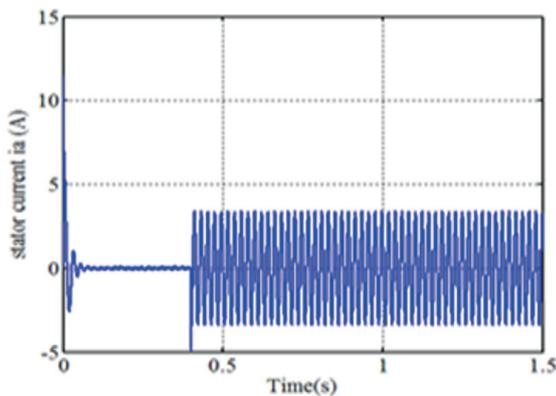


Fig. 11 Waveform of the stator current

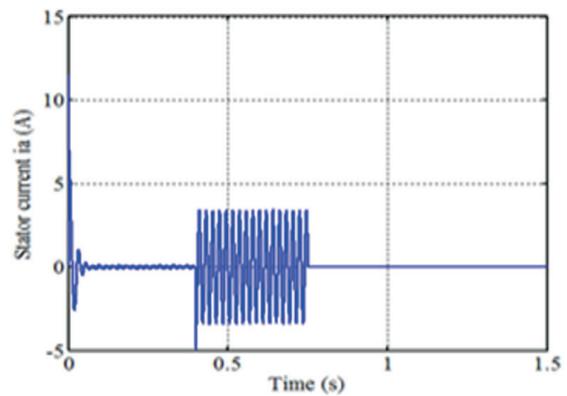


Fig. 14 Wave form of the stator current phase a

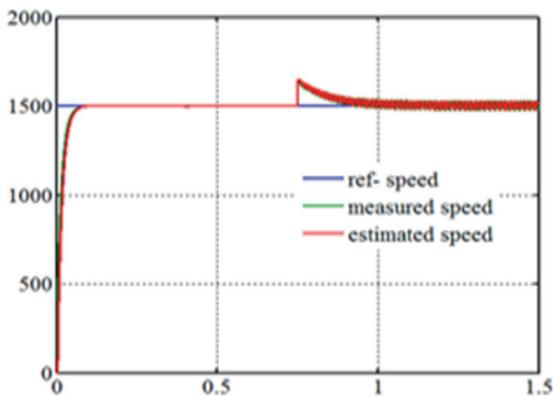


Fig. 12 Waveform of the electromagnetic torque

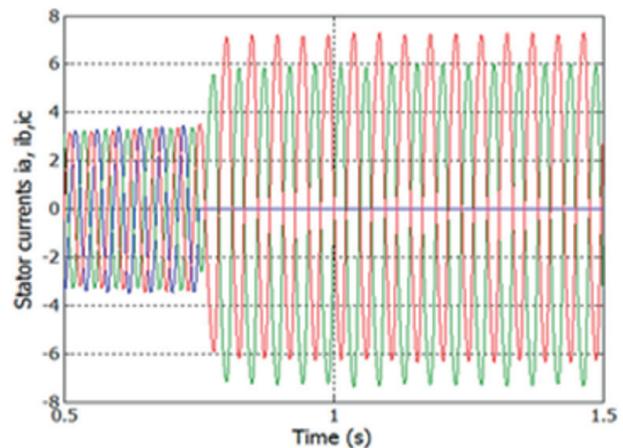


Fig. 15 Wave form of the stator currents phase a,b,c

returns to its nominal value after a few milliseconds (Fig. 17) only when the changeover takes place (response time of the tolerant control faults - time required for diagnosis). We note also large variations in the torque of the machine that accompanies a speed slowdown in (Fig. 18).

This controller is able to tolerate a fault relying on the obtained results during the application of our FTC where there is a conservation of its performance since all the variables return to their nominal states.

8 Conclusion

Eventually, this paper has presented a fault tolerant voltage source inverter, which can compensate faults in the switching devices. A comparison between the behaviors of the machine corresponds to the operation in both the healthy and the degraded modes with the presence and the absence of the fault, has been done. A sensor-less control

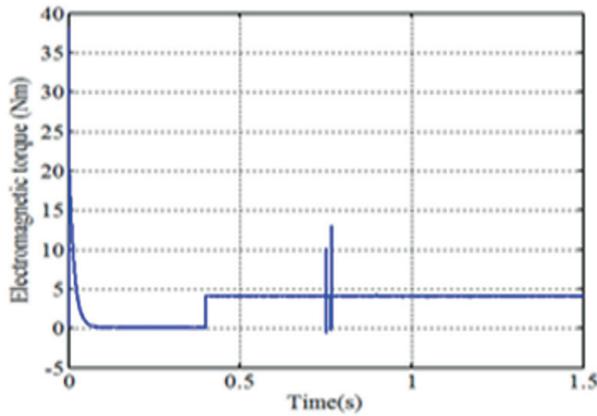


Fig. 16 Wave form of the torque

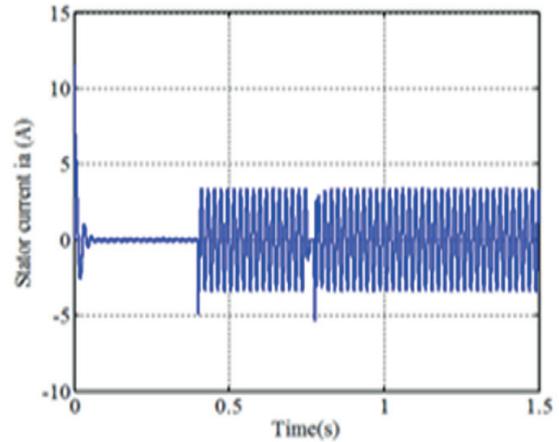


Fig. 18 Wave form of the stator current phase a

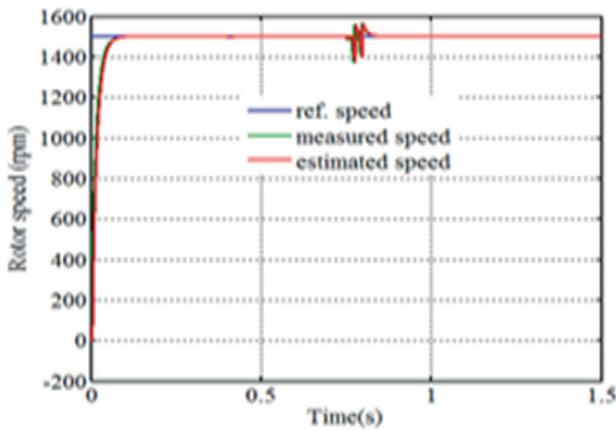


Fig. 17 Wave form of the speed

is based also on MRAS. Thereafter, the simulation results demonstrate that the proposed algorithms have good static and dynamic performances.

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Nomenclature

$d - q$	synchronous axis reference frame quantities
i_d, i_q	stator d and q axis currents
v_d, v_q	stator d and q axis voltages
Φ_d, Φ_q	stator d and q axis flux linkages
L_d, L_q	stator d and q axis inductances
$\hat{\Phi}_m$	peak permanent magnet flux linkage
K_e	Back-EMF coefficient constant
K_t	torque constant
R_s	stator resistance
J	total rotor inertia
f	viscous friction coefficient
p	number of the pole pairs
θ_r	electrical rotor position
ω_r	electrical rotation speed
T_e	electromagnetic torque
T_s	sampling time

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