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RESEARCH ARTICLE

LTCC Based Planar Inductive Proximity Sensor Design

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Abstract

This paper is focused on design and realization of planar inductive sensor system used for proximity sensing based on Low Temperature Co-fired Ceramics (LTCC). Planar coil consisting of six layers was designed, produced and measured. Electronic system for driving coil and processing measured values was developed and realized. Proximity measurement of various metal materials was realized and results were processed and evaluated. Measurements has shown that six-layers LTCC structure with implemented coils in cooperation with developed driving electronic is appropriate solution for design and construction of planar proximity sensor. It had been developed sensitive inductive sensor for up to 7 millimeters distance proximity measurements.

Keywords

planar inductive proximity sensor, planar inductor, LTCC technology

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1 Introduction

Actual trends in electronics industry give demanding requirements on sensors used for process and devices control. Depending of sensing application, immunity against environment impact, reliability and long life cycle, robustness, small physical dimensions, low energy consumption and low manufacturing price are the main requirements for modern sensors and sensing systems. Inductive sensors meet these requirements. Event counting (rotary speed detection, flow meters), simple buttons for industrial keypads, industry switches, metal detection, linear position detection, angle detection, engine tests (valve position), roller gap process control (thickness, shape, texture), quality inspection (deformation, cracks) or vibration sensing are only some of the possible applications of inductive sensors. Because of any mechanical parts, inductive sensors are ideal option for proximity detection.

Harsh environment, low available space and the need of inductive proximity sensing are the main reasons to choose an alternative to standard inductive sensors. Low Temperature Co-fired Ceramic (LTCC) system offers very good alternative for producing planar inductive proximity sensor. LTCC is technology that allows creating of multilayer modules by stacking single ceramic sheets together. Glass-ceramic composite material of LTCC tapes usually consists of Al₂O₃, SiO₂ and organic materials. Sheet of LTCC can be shaped and bended before firing process. LTCC tape processing is based on screen printing, laminating and firing process. Applying of conductive, dielectric and resistive pastes LTCC technology allows to integrate resistors, capacitors and inductors. Resistance against high temperatures and negative impact of given environment [1, 2], ability to produce planar conductors in tenth of micrometer resolution, stacking single ceramic sheets to reduce needed length of coil winding and dimension of the coil itself [3], and an ability to operate in high frequency area predetermines using LTCC as a basic substrate for planar inductor coil. High reliability and stability of realised structures and excellent electrical characteristics [4, 5] predetermine LTCC for use in sensor's applications. Reducing total size of sensing device and increasing reliability of sensing module can be achieved

by integrating sensor's driving electronic system together with planar coil into multilayer LTCC module.

Inductive sensing system is based on penetration of electromagnetic field generated by sensor's coil into target. Own electromagnetic fields that react with the sensor's coil field are generated by currents induced in target material, so minimum considerations on target size and thickness are required [6, 7]. With raising driven frequency minimum thickness of sensed target goes down. Reducing planar coil's dimensions and working at higher frequencies (MHz range) sensing even small and thin conductive targets can be achieved [8].

Principle of inductive sensors' operation allows using these sensors only for metal – based objects sensing. In dependence of sensing coil's area, limited sensing proximity range can be achieved. Inductive sensors consist of sensing coil and driving oscillating circuit.

For manufacturing industry, there is huge potential for inductive sensors especially for process control. When requirements for measuring proximity ranges in few millimetres distance [9], standardly used inductive proximity sensor requires a lot of space for mounting. There had been presented a lot of inductive proximity sensors based on LTCC [1, 3, 10]. The dimensions of mentioned sensors are relatively small (from 4.7x2.4 mm up to 15.7x8.7 mm), but these sensors provides the best sensitivity at micrometre ranges and can be used to measure ranges only up to 4 mm. Because of very small area and high resistance of sensing coils (up to 120Ω), these sensors achieves small quality factor (ratio of stored vs. dissipated energy per unit time). Complex and expensive, but reliable and stable electronic circuits are used to drive these coils.

Design of a compact, multilayer proximity inductive sensor element with small dimensions, but long range sensing distance and universal electronic module for driving inductive sensors and processing measured values is presented in this paper.

2 Planar coil design

Accepting advantages and disadvantages of different coil shapes [11] and also of technological possibilities of LTCC technology for given coil's shape, geometrical parameters of developed planar inductive sensor were determined. To minimize loses and to obtain the best performance of inductive sensor for our application, coil with circle shape shows as the ideal option.

2.1 Coil's parameter calculation

To calculate inductance L of single-layer planar coil of different shapes, Eq. (1) [12] is used:

$$L = K_{1}\mu_{0} \frac{n^{2} d_{AVG} c_{1}}{1 + K_{2}\rho} \left(\ln\left(\frac{c_{2}}{\rho}\right) + c_{3}\rho + c_{4}\rho^{2} \right), \qquad (1)$$

where μ_0 is the permeability of free space, *n* is the number of planar coil's turns, K_1 , K_2 and c_1 to c_4 are constants geometry

dependent on the shape of the inductor (for circle shape, $c_1=1$, $c_2=2.46$, $c_3=0$, $c_4=0.2$), ρ is the coil's fill ratio and is equal to Eq. (2) [12]:

$$\rho = \frac{d_{OUT} - d_{IN}}{d_{OUT} + d_{IN}},\tag{2}$$

where d_{IN} and d_{OUT} is the inner and outer diameter of the coil, respectively, and d_{AVG} is the average diameter of the turns equal to Eq. (3) [12]:

$$d_{AVG} = \frac{d_{IN} + d_{OUT}}{2} \tag{3}$$

Complete calculated parameters of developed coil are listed in Table 1.

Table 1 Complete calculated parameters of developed coil.

Parameter	Value
Outer diameter of coil	15.82 mm
Inner diameter of coil	7.82 mm
Geometric mean diameter	0.338
Number of layers	6
Turns per layer	8
Trace width	0.25 mm
Spacing between traces	0.25 mm
Conductor paste thickness	0.02 mm
Self-inductance per layer	0.954 μΗ
Total inductance	22.556 µН
AC resistance	8.807 Ω
DC resistance	6.107 Ω
Coil length per layer	297.069 mm
Coil total length	1782.414 mm
Spacing between layers	0.2 mm
Coil fill ratio	0.494
Skin depth	0.026
Self-resonant frequency	14.593 MHz
Resonance impedance	25611.29 Ω

2.2 Coil's realization and fabrication

Sample prototype coil with parameters listed in Table 1 was fabricated using DuPont 6145 silver co-fireable conductor paste screen printed on DuPont GreenTape[™] 951PX ceramic sheets with 254 µm thickness. After isostatic lamination (water temperature of 70°C, pressure of 20.68 MPa) for 10 minutes, coil was co-fired using recommended [13] 3.5 hours co-fire profile with 850°C maximum temperature for 20 minutes. Sensor's coil has circle shape with 15.82 mm diameter, 250 µm conductor's width and spacing between conductors and consist of six layers. Printing of coil's conductor with even small dimensions was not affected by "moiré pattern". Top side's topology of the developed planar coil as one part of 6 layers structure design is presented in Fig. 1. The whole topology of developed coil is shown in Fig. 2.



Fig. 1 Developed coil for use in inductive proximity sensor.



Fig. 2 Internal structure of developed six-layers planar coil (red color - vias connecting two layers, blue color - vias via all six layers).

2.3 Coil's characterisation

After proper final inspection, electrical parameters characterisation of developed coil was performed. We decided to use SMA connector to limit parasitical effects of connection to measurement device. There had not been placed additional capacitor on sensing coil during measurement process. Inductance of coil in the frequency range from 300 kHz to 15 MHz was measured by vector network analyser (VNA) N5231A by Keysight Technologies (Fig. 3). Fluctuations in Fig. 3 are caused by measurement step of used VNA. At frequencies higher than 14 MHz parasitic effect of capacitance given by planar structure of coil appears that limits the use of this coil at higher frequencies. Optimizing coil's shape to minimize resistance causing loses and to obtain best performance, developed coil reaches the quality factor of 3, that is a good value for sixlayer planar coil.



Fig. 3 Developed planar coil's inductance in dependence of driving frequency.

3 Design of driving electronic module for planar coil

Inductive sensor for its operation requires driving circuit. Based on performance of driving circuit, behaviour of whole sensing system can be determined. Proper considerations should be taken for choosing appropriate driving circuit to obtain stable and sensitive inductive sensor.

There are several possibilities to drive an inductive proximity sensor, every with its advantages and disadvantages [14]:

- crystal or oscillator of fixed value. Using crystal or oscillator of fixed value brings advantages of simple circuit design and frequency and temperature stability. To reach defined oscillation frequency, an inductor or capacitor tuning is required. When another oscillator frequency is needed, new driving electronic circuit must be build. Another electronic system (e.g. microcontroller) is needed for processing measured values.
- Collpits, Clapp or Hartley oscillators. These types of oscillators are known for wide frequency range and frequency stability [15].
- demodulation circuits, such as frequency modulation (FM), amplitude modulation, phase detection and balanced bridge [9]. High resolution, linearity, high frequency response and low noise are the main advantages of using FM.
- inductance to digital converters (LDC's.).

Inductance to digital converter was considered as an ideal option for purpose of driving a developed coil.

3.1 LDC based driving electronic module

Inductance to digital converter is the device that simultaneously measures resonant frequency and impedance of connected parallel LC resonant circuit. Oscillation amplitude of resonant circuit is regulated to a constant level in a closed-loop configuration, and by monitoring power injected into resonant circuit, parallel resistance R_p of the coil is determined. By measuring oscillation frequency of resonant circuit, inductance of resonant circuit is determined. LDC's are available in a wide range of mounting packages and configurations [16]:

- 1/2/4 input channels,
- 3,3V/5V operation voltage (analog + digital),
- I2C/SPI interface,
- 12/24/28 bits inductance resolution,
- 8/16 bits parallel resonance impedance resolution,
- 1.8V up to 4V oscillation amplitude,
- 1 kHz to 10 MHz / 5 kHz to 5 MHz / 300 kHz to 19 MHz sensor frequency,
- parallel resistance range from 798 Ω to 3.93 M\Omega,
- implemented programmable comparator,
- catalog or automotive rating.

With minimum external components required, LDC's provides a reasonable solution for inductive sensing from the view of reliability and all-in-one chip solution. For our proximity sensing application, Texas Instruments LDC1000 inductance to digital converter was chosen. Detail specifications of this device are listed in Table 2. Functional block diagram and typical application of LDC1000 inductance to digital converter are presented in Fig. 4 and Fig. 5, respectively. ATmega328 - based microcontroller circuit is used for processing of measured values and communication with computer. To allow using developed driving system with a wide range of different sensing coils, simple program for calibration before every start of sensing application was written. For proper operation some of the LDC1000's configurations registers must be especially configured.

Table 2 Texas Instruments LDC1000 Inductance to Digital	
converter specifications [17]	

Parameter	Value
Number of channels	1
Supply voltage (analog, digital)	5V
Interface	SPI
Inductance resolutions	24 bits
Oscillation amplitude	$1 \mathrm{V} - 4 \mathrm{V}$
Sensor frequency	5 kHz – 5 MHz
Parallel LC circuit resonance range	798 Ω - 3.93 ΜΩ
Parallel resonance impedance resolution	16 bits
Rating	automotive



Fig. 4 Functional block diagram of LDC1000 [17].

3.2 LDC1000 inductance calculations

There are two values that can be read from LDC1000 using SPI communication – proximity data (PD) and frequency data (FD). To calculate inductance L of the coil, Eq. (4) [17] is being used:

$$L = \frac{1}{C \cdot \left(2 \cdot \pi \cdot f_{sensor}\right)^2},\tag{4}$$

where C is the parallel capacitance of the resonator and f_{sensor} is the sensor frequency equal to Eq. (5) [17]:

$$f_{sensor} = \frac{1}{3} \cdot \frac{f_{ext}}{f_{count}} \cdot t_{res},$$
(5)

where f_{ext} is the external clock's frequency, f_{count} is obtained FD and t_{res} is the programmed response time.

Equation (6) [17] is used to calculate resonance impedance R_p of parallel resonant circuit from obtained PD:

$$R_{P} = \frac{R_{P} MAX \cdot R_{P} MIN}{R_{P} MIN \cdot \left(1 - \frac{PD}{2^{15}}\right) + R_{P} MAX \cdot \frac{PD}{2^{15}}},$$
(6)

where $R_{p}MAX$ and $R_{p}MIN$ are programmed maximum and minimum R_{p} that LDC1000 must measure, respectively. These parameters configure the input dynamic range of this device.



Fig. 5 LDC1000's typical application [17].

3.3 Results and discussion

Complete developed LTCC inductive proximity sensor is presented in the Fig. 6. Sensing coil and electronic module are connected using SMA cable.



Fig. 6 Complete developed LTCC - based inductive proximity sensor.

Measurements of axial proximity according to Fig. 7 were done to characterize developed inductive proximity system. To obtain comparable results according of inductive proximity sensing requirements [16], these measurements were done with three targets of different material, but thickness of every material was at least 3 mm and the area of used targets was at least twice in compare of sensing coil's area.



Fig. 7 Principle of inductive proximity sensing measurement. [16]

Measured values of PD and FD depending on distance from target are presented at Fig. 8 and Fig. 9, respectively. Calculated values of parallel resistance R_p and inductance L of developed coil are presented at Fig. 10 and Fig. 11, respectively. These measurements were done with three different target materials – aluminium, solder material and copper.



from target for three different targets.



Fig. 9 Measured FD (in thousands) in dependence of distance from target for three different targets.



Fig. 10 Calculated parallel resistance R_p of developed coil in dependence of distance from the target for different targets.



Fig. 11 Calculated inductance L of developed coil in dependence of distance from target for different targets.

At Fig. 8 to Fig. 11 it can be seen, that for distances from 4 mm to about 10 mm developed inductive proximity sensior is able to recognize targets from different materials. After the distance of 10 mm is overreached, inductive sensing system is only able recognize presence of metal based target.

Sensor shows the best performance for copper material target. Targets from aluminium and solder material show very similar performance. These differences are caused by different permeability value of used target materials.

The best sensitivity of planar inductive sensor is in the distance range from 4 mm to 7 mm. For the measuring distances under 3 mm, sensor must be recalibrated. Measurements showed instability of LDC's output values when measuring proximity range. This instability was caused by improper placement of LDC's driving circuit placed on microcontroller board. To improve stability, driving circuit should be placed directly to sensing coil without necessary long traces or even cables. Using 28-bits driving circuit instead of 24-bits even better sensitivity can be obtained.

Chosen LDC-based electronic system showed electrical characteristics comparable with much complex and far more expensive circuits required for driving inductive proximity sensors. Based on combination of used LTCC technology and allin-one driving chip solution, integration of both components at one substrate can be done to obtain highly reliable, parametric stable and price reasonable inductive sensor.

Developed planar inductive sensor can be used for applications, where copper material target has to be detected. In these sensing applications, recommended proximity sensing distance is 4 to 7 mm.

4 Conclusion

In this paper, compact inductive proximity sensing system based on LTCC was introduced and characterized. Using six-layer planar coil with 15.82 mm diameter we were able to measure up to 20 mm proximity distance of target.

Inductance to digital converter was confirmed as a reasonable solution for driving inductive sensor. This type driver and planar inductive sensor combination showed performance comparable with much more complex and expensive driving solution. Integrating LDC converter directly at sensing coil substrate, a very stable, small dimension and highly reliable planar inductive sensor can be achieved.

Measurements showed that same physical dimensions targets, but of different materials do not behave the same for inductive sensor. Because of that, introduced inductive sensor can be used for target material characterization in limited proximity distance range. The best sensitivity of presented inductive sensor was measured for distances up to 10 mm, repeatability measurement was verified for target distance from 4 to 7 mm.

Developed inductive proximity sensing system will be used for education purposes in sensor's field. Because of ability to drive a coil in a wide frequency range, used driving electronic system will be the base for our future work.

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